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Persulfate-based advanced oxidation processes: The new hope brought by nanocatalyst immobilization

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1 Abstract:

Persulfate-based advanced oxidation processes (persulfate-AOPs) offer great promise for 2 environmental remediation, with heterogeneous catalysts providing the backbone of 3 many wastewater purification technologies. Unlike conventional nanocatalyst 4 5 heterogeneous systems, the immobilized-catalyst system can bypass the separation 6 problem to reduce scour and prevent aggregation by anchoring nanoparticles onto porous or large-particle carriers. This review presents the state-of-the-art of knowledge 7 8 concerning immobilization methodologies and reactors, reaction mechanisms, and activation performance. Immobilization techniques onto supports are summarized and 9 10 discussed, including membrane-based reaction systems (immersion mode, and filtration mode), electrocatalytic auxiliary systems, and alternative supports (metallic glasses, 11 12 aerogels, hydrogels, and specific materials). Key scientific problems and important prospects for the further development of immobilized catalysts are outlined. 13

14 Keywords: advanced oxidation process; nanocatalyst immobilization; persulfate;
15 wastewater treatment

Full Text	Abbreviation
Persulfate-based advanced oxidation processes	persulfate-AOPs
Advanced oxidation processes	AOPs
Reactive oxygen species	ROS
Peroxymonosulfate	PMS
Peroxydisulfate	PDS
Reduced graphene oxide	rGO
Polyvinylidene fluoride	PVDF
Polyacrylonitrile	PAN
Scanning electron microscope	SEM
S, N-doped carbon and iron nanoparticles	NSC-Fe
Layered double hydroxides	LDH
Nanofibers	NFs
Metal-organic frameworks	MOFs
Cellulose nanofibers	CNFs
Electrospun nanofibers	ENFs
Zero-valent iron	ZVI
Metallic Cu-doped C/SiO ₂ nanofibers	CINMs
Ag-La _{0.8} Ca _{0.2} Fe _{0.94} O _{3-δ}	Ag-LCF
Zeolitic imidazolate framework	ZIF
Calotropis gigantea fiber	CGF
Carbon nanotubes	CNTs
N-doped microtubule composites/PVDF	CFP
Biomimetic polydopamine	PDA
Polypropylene	РР
Total dissolved solids	TDS
Poly tetrafluoroethylene	PTFE
Metallic glass(es)	MGs/MG
Ultraviolet-visible light	UV-Vis
Three-dimensional	3D
Co-doped carbon aerogels	CoCA
Selective laser melting	SLM
Isotropic CoFe ₂ O ₄ @graphene hybrid aerogel	CFO@GA-I
Anisotropic CoFe ₂ O ₄ @graphene hybrid aerogel	CFO@GA-A
Graphene hybrid aerogel	GA
Polyacrylic acid	PAA
Graphene oxide	GO
Chemically bonded Co ₃ O ₄ nanoflowers sponge	SP-50
Double-network hydrogel templated FeS/graphene	DMG
Polyvinyl alcohol	PVA

TiO ₂ nanotubes	TNTs
CoFe ₂ O ₄ on quartz sand support	CoFe ₂ O ₄ -QS
In situ chemical oxidation	ISCO
Capacitive deionization	CDI
Multiwalled carbon nanotube	MWCNT
Activated carbon fiber	ACF
Electro PDS	E-PDS
Electro PMS	E-PMS
Carbon fiber paper	CFP
Carbon fiber	CF
Flow-through cathode	FTC
Flow-by cathode	FBC
Asymmetric quasi capacitive deionization	AQCDI
Covalent organic frameworks	COFs
Natural organic matter	NOM
Polyethersulfone	PESF
1-methyl-2-pyrrolidinone	NMP
CoFe alloy and CoFe ₂ O ₄ encapsulated in N-doped microtubes	CoFe-NMTs
Carbon black nano-spheres	CBNS

18 **1. Introduction**

19 The importance of water safety for economic development and public and environmental health cannot be overstated. Yet, despite rising levels of contamination 20 and salinity of inland freshwater [1], more than 650 million people currently lack access 21 to safe water [2]. Common natural pollutants, including pathogenic microorganisms, 22 23 earth-derived heavy metals, cyanobacterial toxins, and metal-like substances (e.g., arsenic), can be removed through traditional water treatment methods (i.e., filtration 24 and precipitation) [2]. However, the application of these basic technologies is limited 25 by throughput requirements. Furthermore, priority pollutants and emergent 26 27 contaminants have been found in natural streams, drinking water sources, and even 28 sewage treatment plant effluents, thus posing a threat to human and ecosystem health. This is exacerbated by the proliferation and discharge of multidrug-resistant bacteria in 29 certain sewage treatment plants, leading to health risks and reduced productivity [3-5]. 30 The foregoing highlight the need for technological innovation and resilience to improve 31 32 inefficient water treatment infrastructure.

Advanced oxidation processes (AOPs) provide a powerful means of degrading and even mineralizing refractory organic pollutants through the induction of reactive oxygen species (ROS), thus avoiding the need for further treatment of contaminantladen sorbents or membrane concentrate streams [6]. In general, hydroxyl radicals (•OH) [7, 8], sulfate radicals (SO4⁺⁻) [9, 10], chlorine radicals (Cl• and Cl2⁺⁻) [11, 12], and radicals that enable direct electron transfer possess [13] can achieve rapid

39 decomposition of various organic pollutants and pathogenic bacteria. Owing to their lack of pH dependency and selective oxidation, persulfate-based advanced oxidation 40 41 processes (persulfate-AOPs) have begun to receive more research attention than standard Fenton systems. Nanomaterials have provided an immense impetus as 42 heterogeneous catalysts for peroxymonosulfate (PMS, 2KHSO₅·KHSO₄·K₂SO₄) and 43 44 peroxydisulfate (PDS, $Na_2S_2O_8$ or $K_2S_2O_8$) activation. The key mechanism behind the persulfate heterogeneous activation reaction is the direct transfer of electrons from 45 catalysts to persulfate ions (labeled as "Radical mechanism" in Fig. 1). Researchers 46 47 have recently proven the existence of a non-radical oxide pathway (marked as "Nonradical mechanism" in Fig. 1), involving a direct electron transfer process, reaction with 48 surface-activated complex (or surface-confined radical), direct oxidation of high-49 50 valence metals, and the participation of singlet oxygen in the catalytic oxidation of organic contaminants [14-16]. 51



52

Fig. 1. Heterogeneous activation mechanism of persulfates, and challenges to nanocatalysts in persulfate based-AOPs.

55 However, nanocatalyst loss to product water, mass transfer limitations, ROS

56 oxidative attack, and breakage under intense shear are almost inevitable in a nanoparticle catalytic system [17, 18]. Although nanotechnology cannot solve all water 57 58 treatment problems, nanomaterials might enable the development of next-generation engineered water purification systems, which are compact and simple to deploy [2, 19]. 59 60 Immobilization has recently been reported to help minimize leaching, inducing an 61 obvious degradation effect and reducing the cost associated with separation of 62 nanocatalysts, thus leading to more effective application of nanoparticle-based AOPs for water remediation [20-22]. The future development of persulfate-AOPs depends on 63 64 the optimization and immobilization of nanocatalysts in addition to reactor design. For instance, reduced graphene oxide doped with nitrogen/polyvinylidene fluoride matrix 65 (rGO-N-PVDF) composite membrane was prepared and used in a specific filtration 66 67 system with compact structure, convenient operation, and easy recovery in water treatment [23]. Conversion of pharmaceuticals in the range 54%-91% was then 68 obtained even after 24 h of operation in full continuous mode, thus demonstrating the 69 activation performance of rGO-N-PVDF for PDS conversion. However, the pollutant 70 71 removal efficiency decreased in preliminary experiments using surface water compared 72 to those using ultrapure water. Therefore, this research field presents both opportunities 73 and challenges, requiring more comprehensive scientific research in the future. Simultaneous specific reaction systems and reactors have recently been 74

reaction systems and reactors have recently been reaction systems and reactors have recently been reaction systems and reactors have recently been reaction system formed from composite material and a synergistic filtration system, as shown in **Fig. 2**. These can be directly supplemented with light and heat sources to achieve more efficient, faster wastewater

treatment [16, 24, 25]. Nevertheless, specially designed reactors are required in 78 electrocatalytic auxiliary systems (examples shown in Fig. 2). This review describes 79 the current state of knowledge of persulfate activation methods, different 80 immobilization methodologies and reactors, reaction mechanisms, and activation 81 performance. Challenges and future prospects are discussed, including the lack of a 82 83 universal optimization principle for catalyst preparation and reactor design, and the use of blank standardized experimental methods in various complex water matrices which 84 ignore cost and life-cycle effects. The overall goal is to gain insight into design 85 approaches for next-generation multifunctional treatment systems that reduce water 86 pollution and energy consumption. 87



88

89 Fig. 2. Construction strategy for persulfate activation systems based on immobilized nanocatalysts.

90 2. Membrane-based reaction systems

91 2.1 Immersion mode reaction systems

92 The working pH in a PMS activation system is harsh; thus, the standards for catalyst stability and raw membrane material are higher compared to other systems. 93 94 Moreover, maintenance of catalytic performance relies on the redox reaction (i.e., metal valence state transformation), whereas very strong nanoparticle-support interactions 95 between the support and nanoparticles usually make it difficult to reduce nanoparticles. 96 Based on their superior characteristics in terms of long life-span, thermal stability, and 97 excellent tolerance to pH, ceramic membranes have attracted much attention in recent 98 99 years, as summarized in **Table 1**. For example, the composite membrane covered with polyacrylonitrile (PAN)-Co-C and a Co/C layer shown in Figs. 3(a-1)-(a-4) has a 100 porous surface and cross-section [26]. The catalysis performance of such membranes 101 102 has been ascribed to abundant active functional sites (C, N, and Co), thus importing an intrinsic antifouling effect in the membrane filtration process. The formation of a 103 chemical bond between the C/Co layer and Al₂O₃ results in more robust functionalized 104 105 membranes with stable catalytic performance. However, these ceramic membranes are extremely brittle, which means that they can easily break and disperse during 106 application. Moreover, the fragments are difficult either to collect or to recover. 107



108

109 Fig. 3. Typical composite membrane prepared via ceramic and polymeric substances, and then used in 110 immersion mode reaction systems: (a) synthetic procedure for PAN-Co ceramic membrane, with SEM 111 surface images of (a-1) initial Al₂O₃ membrane, and (a-2) functionalized PAN-Co-C membrane, and 112 SEM cross-section images of (a-3) initial Al₂O₃ membrane, and (a-4) functionalized PAN-Co-C 113membrane (reprinted with permission from [26], copyright 2019 Elsevier); (b) synthetic procedure for 114LDH@PVDF membrane (reprinted with permission from [27], copyright 2020 Elsevier); and (c) 115synthetic procedure for NSC-Fe@PVDF membranes, with (c-1) digital photograph of NSC-Fe@PVDF 116 membrane and (c-2) color changes of Orange II in NSC-Fe@PVDF/PMS system (reprinted with 117 permission from [28], copyright 2017 Elsevier).

Generally, polymeric substances are easy to synthesize and manufacture; thus, they play an important part in nanocatalyst immobilization. In particular, composite membranes fabricated via polymeric substances show great suppleness, which means that they can be collected and washed using a simple treatment process (see **Table 1**) to achieve recycling of catalytic materials. Polyvinylidene fluoride (PVDF) is a 123 promising membrane substrate that features: (i) great physical and chemical stability, allowing it to be applied under a wide range of conditions; (ii) excellent flexibility, 124 125 enabling it to be processed into different shapes; and (iii) cost-effectiveness and ecofriendliness. As shown in Figs. 3(b) and (c), hybrid catalytic PVDF membranes are 126 readily fabricated by the phase inversion technique. For instance, the functionalized, 127 128 pure, white PVDF membrane appears black after being doped by iron nanoparticles embedded in S, N-cooped carbon (Fig. 3(c-1)), demonstrating a uniform distribution of 129 nanocatalysts [28]. The synergistic effect between S, N-doped carbon, and iron 130 131 nanoparticles (NSC-Fe) improves the catalytic ability of NSC-Fe@PVDF; thus, substantial decolorization of orange II occurs with low metal leaching (Fig. 3(c-2)). 132 Table 1 lists data that confirm the great activation performance and durability of layered 133 134 double hydroxides (LDH)@PVDF and the CuO@CuS/PVDF membrane.

During the heterogeneous catalytic reaction, the degradation effect of target 135 pollutants correlates positively with the interaction between PMS and catalyst. 136 Therefore, catalyst with high specific surface area and porosity is required, in order to 137 promote interaction with PMS [29]. Nanofibers (NFs) are widely considered to be a 138 139 promising support for nanoparticle immobilization because of their high surface area. Generally, nanocatalysts immobilize uniformly and tightly on the surface of NFs when 140 exposed to reactants, such as oxidizing agents, contaminants, and coexisting ions or 141 organic matter [27, 30]. With their large continuous surface area and high flexibility, 142 NFs can form random arrays and macroscopic mats, which are beneficial for catalyst 143 separation, recovery, and reuse [31]. Fig. 4(a) illustrates vacuum filtration, an efficient 144





Fig. 4. Typical composite membrane prepared from nanofibers through filtration, and used in immersion mode reaction systems: (a) synthetic procedure, (b) SEM image of Co/Fe bi- MOFs/CNFs membrane (reprinted with permission from [32], copyright 2020 Elsevier); and (c) schematic representation of magnetic nanocellulose membrane preparation and PMS activation process (reprinted with permission

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163 from [33], copyright 2020 Elsevier).

Thus far, owing to the absolute discontinuity of nanoparticles, the mechanical 164 165 properties of the foregoing composite membrane prepared by vacuum filtration are much lower than those of existing advanced fiber-reinforced composites [34, 35]. 166 Electrospinning is a technique that produces continuous NFs by jetting polymer 167 solutions in high electric fields, thus providing excellent control over NF dimensions 168 169 and orientation, as illustrated in Fig. 5(a) [36]. Compared with nanofibers synthesized using other methods, electrospun nanofibers (ENFs) provide overwhelming benefits, 170including: (i) potential for controllable synthesis; (ii) large specific surface area, high 171 aspect ratio, and oriented charge transfer pathways; (iii) excellent compositional and 172structural stability; and (iv) cost control of mass production, especially for 173 multicomponent composite fibers, suitable for industrial application [37]. A previous 174 175study synthesized composite α -Fe(α)carbon ENFs by co-electrospinning and pyrolysis 176 self-reduction [38]. In Fig. 5(a), small particles of average diameter ... nm could be 177 observed on the surface of the fiber, demonstrating that iron species were distributed uniformly and welded firmly in the fibrous scaffolds. Based on active zero-valent iron 178 (ZVI), the ENFs exhibited excellent PMS activation activity, high stability, and easy 179 magnetic separation during the contaminant removal process. However, the flexible 180 181 ENF membranes (nonporous or microporous, < 2 nm) were unable to provide sufficient active sites for pollutant adsorption and ROS transportation, thus limiting further 182 improvement in catalytic capability [39, 40]. 183



184

Fig. 5. Typical composite membrane prepared from electrospun nanofibers, and used in immersion mode reaction systems: (a) synthetic procedure for metallic Cu-doped C/SiO₂ nanofibers (CINMs) by sol-gel electrospinning method; (b) SEM image of α -Fe@carbon ENFs (reprinted with permission from [38], Copyright 2017 RSC); (c) SEM image of CINMs; and (d) optical photograph showing that the CINMs could be folded into a paper crane without any fracturing (reprinted with permission from [39], copyright 2019 RSC).

A recent study of inorganic membranous catalysts that have extraordinary flexibility and large mesopores by Shan et al. [39] has provided convincing evidence for the improvement of their catalytic oxidation activity in persulfate-AOPs. Shan et al. successfully fabricated $Cu@C/SiO_2$ nanofiber membranes (CINMs) through electrospinning and *in situ* carbonization (**Figs. 5(c)** and **(d)**). As indicated in **Fig. 5(c)**, the synthesized nanoparticles were able to break through the ground and become firmly fixed on the NFs surface, indicating the structural stability of the resultant membranes and the validity of the electrospinning method. Furthermore, the as-obtained CINMs, which have large mesopores and are very flexible, can withstand large bending and torsional deformations with no detectable fractures (see **Fig. 5(d)**). This synthetic strategy therefore overcomes the obstacles of brittleness and the poor mechanical properties of crystalline inorganic NF membranes, and can be further extended to other metal-embedded inorganic membranes.

The integrated effect of randomly arranged NFs, sufficient hydroxyl groups, and 204 rough surfaces of nanostructures endows synthesized CINMs with superhydrophilicity, 205 206 a property conducive to water purification. Furthermore, as indicated in Table 1, novel Co-Al₂O₃ and Pt-Al₂O₃ NFs membranes prepared using electrospinning have 207 demonstrated great flexibility and excellent PMS activation capability [41, 42]. Given 208 209 its flexible membrane form, the shape of Pt/Al₂O₃ can be adjusted for use in different membrane reactors [42]. As for the reaction mechanism, PMS can be easily adsorbed 210 on the surface of Pt/Al₂O₃ fiber through its oxygen atom, due to the positive charge of 211 212 Pt/Al₂O₃ during the reaction process. Meanwhile, electron-rich organic molecules with aromatic rings in the structure may also be adsorbed on the fiber and contribute 213 electrons to PMS through Pt as a medium, thereby leading to further destruction of 214 organic pollutants and gradual decomposition of PMS. 215

Ma et al. [43] processed Ag-La_{0.8}Ca_{0.2}Fe_{0.94}O_{3- δ} (Ag-LCF) into hollow fiber membranes by means of a phase-inversion and sintering method. They examined the reaction of the Ag-LCF hollow fiber membrane, whereby a methylene blue and persulfate solution was pumped into the fiber lumen at a prescribed flow rate. SEM images revealed pinhole defects and exposed particles that appeared on the inner surface with increasing grain size (see inset). The membrane wall, especially the dense membrane core, was kept intact to prevent wastewater from leaking from the cavity into the shell side. However, further measurements are still needed, including the mineralization efficiency of pollutants, metal leaching concentration, reusability, and active sites of Ag-LCF.

From the above collection of mixed systems based on catalytic membranes, a 226 possible reaction mechanism has been identified, as depicted in Fig. 6 [28, 32]. First, 227 pollutant and persulfate ions (i.e., HSO_5^- and $S_2O_8^{2-}$) adsorb on active sites on the 228 membrane surface. Next, surface adsorbed persulfate is activated by catalytic sites to 229 induce ROS, and then interacts with adsorbed organic molecules and/or bacteria 230 231 through an in situ reaction, after which the preoccupied sites are released. These released free sites accelerate the transfer of aqueous reactant, thereby initiating a new 232 adsorption-oxidation cycle. The foregoing cycle repeats itself until most or all of the 233 target pollutants are removed. The nano-size effect of metal particles and the relatively 234 low diffusion resistance of organic matter on the surface of catalytic membranes are 235 conducive to full contact between organic matter and active sites, which is beneficial 236 to the catalytic performance of the membrane [28]. For carbon-based and carbon-doped 237 catalytic membranes, the work function of metal nanoparticles embedded in carbon is 238 lower than that of a carbon surface due to facile electron transfer from the metallic 239 active sites to the carbon atom [44]. At the same time, the carbon shell forms a reservoir 240 that effectively delays the process of iron dissolution (in the solution). Hence, such 241

composite membranes intrinsically display enhanced stability and excellent catalytic performance. However, organic molecules and persulfate ions experience difficulty in entering the catalytic membrane pores in batch mode (**Table 1**), which prevents full utilization of the possible active sites in the membrane pore walls (see **Fig. 2**). An alternative approach is to assemble the composite membranes in the filtration reactor, enabling the internal active sites to be properly exploited.





Fig. 6. Schematic illustration of reaction mechanism for organic removal by (a) Co/Fe bi-MOFs/cellulose
 NFs membrane/PMS system (reprinted with permission from [32], copyright 2020 Elsevier), and (b)
 NSC-Fe@PVDF/PMS system (reprinted with permission from [28], copyright 2017 Elsevier).

252 2.2 Filtration mode reaction systems

Persulfate-AOPs can be used in conjunction with membrane filtration as a
 pretreatment stage to degrade organic compounds in the membrane feed stream. This

serves as a mixed/one-pot process and a post-treatment stage to demineralize nonrejected micropollutants in the infiltration stream and reduce organics in the concentrated liquid stream. It has been demonstrated that this series of combined processes (i.e., the filtration system in **Fig. 2**) can efficiently remove pollutants [45]. These treatment methods represent the latest developments in the field (**Table 2**). The following section discusses several advanced studies on the coupling of membrane filtration and persulfate-AOPs.

Wang et al. [46] established an in situ growth technique to produce a zeolitic 262 263 imidazolate framework (ZIF)-67/PAN filter, in which the loading ZIF-67 retained its morphology, structure, and catalytic capacity in comparison to pure ZIF-67 powder. It 264 has been confirmed that Co²⁺ in ZIF-67 can activate PMS to generate ROS for pollutant 265 degradation. Moreover, a piece of ZIF-67/PAN filter (3.5 cm²) can be installed in the 266 Swinnex syringe filter bracket enabling the syringe pump to drive contaminated 267 solution through the filter, achieving water purification (Fig. 7(a)). Likewise, CuCo 268 269 LDH@PAN and CuCo LDH@calotropis gigantea fiber (CGF) composite membranes have been synthesized through vacuum filtration (Fig. 7(b)) by our group to enhance 270 the applicability of highly efficient nanocatalysts [27]. In Fig. 7(b) the pure CGF 271 membrane sample is white, and the composite membrane has a generally brown color, 272 indicating a uniform distribution of CuCo LDH on the CGF scaffold. The morphology 273 of the membrane surface changed visibly after the CuCo LDH coating, also indicating 274 successful fabrication of the composite membrane. Results of controlled experiments 275 revealed that the remarkable catalytic performance of both LDH@CGF and 276

277 LDH@PAN can be attributed to the excellent PMS activation capability of CuCo LDH. Nevertheless, the metal iron leaching property and stability of composite membranes 278 279 with different nanocatalysts and/or supports warrant further, in-depth investigation. The activation ability of catalytic membranes in dead-end filtration mode has been 280 281 tested through full recirculation of the filtrate. Fig. 7(c) presents the recirculation mode 282 as configuration A, and the continuous (non-recycling) mode experiments as configuration B [23, 47]. In the recycling filtration mode, the filtrate entered the feed 283 tank under vigorous stirring, and samples were taken each membrane filtration cycle. 284 By adjusting the transmembrane pressure and residence time, the nanocomposite 285 membranes were able to control the degree of reaction in a manner that was easy to 286 operate. As a key characteristic of membrane filtration [48], water flux is intimately 287 288 linked to surface and structural features of the filter layer, which impact treatment efficiency and energy consumption during operation. Sheng et al. [51] illustrated that 289 the water flux of the composite membrane increases in accordance with enhancement 290 291 of the C/O ratio of the GO/carbon nanotubes (CNTs) mats, with the ratio exhibiting a linear relationship with the reduction degree of rGO flakes (Table 2). Furthermore, Fan 292 et al. [49] reported a new integrated system for phenol removal by combining a coal-293 based carbon tube membrane with persulfate-AOPs. 294



295

296 Fig. 7. Typical composite membranes used in filtration mode reaction systems based on vacuum filtration: 297 (a) synthetic procedure, SEM images, and water treatment method for ZIF-67/PAN membrane (reprinted 298 with permission from [50], copyright 2017 Elsevier); (b) synthetic procedure, SEM images, digital 299 photos and water treatment method for CoCu LDH-CGF membrane and pristine CGF membrane. 300 (reprinted with permission from [27], copyright 2020 Elsevier); and (c) schematic diagram of the 301 experimental setup under recirculation mode (configuration A) and continuous mode (configuration B). 302 (reprinted with permission from [23, 47], copyright 2019 and 2020 Elsevier); the digital photograph 303 depicts elements in the filtration reaction system with recirculation and continuous modes (reprinted with 304 permission from [51], copyright 2020 Elsevier).

However, composite membranes prepared by vacuum filtration have poor mechanical properties, which adversely impact on their long-term use in practice. As a possible solution, high-efficiency nanocatalysts with CoFe alloy and CoFe₂O₄ 308 encapsulated in N-doped microtubule composites were fabricated and immobilized into [52]. The CFP 309 PVDF (CFP) membrane membrane exhibited excellent superhydrophilicity and high flux (1 463.7 L/(m·h·bar), in accordance with SEM 310 images (Fig. 8(a)). The foregoing indicate that the powder catalysts served as pore-311 forming agents to the PVDF membrane, thus allowing electrons to be transmitted 312 313 quickly without being affected by high mass transfer resistance. As evident in Table 2, the CFP membrane achieves excellent, stable catalytic performance and low metal 314 leaching. After adding PMS, the CFP membrane not only maintained a high removal 315 316 rate of tetracycline degradation (more than 90%) in the humus coexistence system but 317 also effectively eliminated the adverse effects of membrane pollution, thus demonstrating that the membrane possessed an excellent catalytic self-cleaning 318 319 property. As illustrated in Fig. 8(b), biomimetic polydopamine and ZIF-67 decorated polypropylene (PDA/ZIF-67@PP) membrane under Xenon lamp irradiation were 320 filtered with feed solution consisting of contaminants and PMS at 1 bar pressure [53]. 321 322 Abundant active sites, such as carboxyl, amide, and phenolic hydroxyl occur in the PDA layer, which can bind with Co ions during synthesis of ZIF-67. As a result, the 323 membrane exhibited especially desirable properties of recyclability, antifouling, and 324 self-cleaning during pollutant degradation. Hence, integration of catalytic oxidation 325 technology with membrane technology offers a broad prospect for overcoming fouling 326 [52, 53]. 327

328 Another alternative water treatment unit design strategy is based on a fluidized 329 bed. Zhu et al. [54] demonstrated that an optimized α -Fe₂O₃ nanodisk/bacterial 330 cellulose composite membrane attained excellent PMS photodegradation performance in both ordinary stirring and flowing bed states (Fig. 8(c)). Rich hydroxyl groups on 331 332 the bacterial cellulose benefited the accommodation and dispersion of α -Fe₂O₃ nanodisks and helped enrich dyes on the surface. Furthermore, the membrane retained 333 334 high catalytic efficiency, especially in the flowing bed condition, and achieved long-335 term durability over a range of flow rates. Compared to batch mode operation, the Fe_xO_v functionalized membrane/PDS system has been found to have higher degradation 336 efficiency in the pressure filtration mode, as shown in Fig. 8(d) pathway A [55], and 337 that the diffusion resistance of the reactants limited accessibility of Fe_xO_y located in the 338 membrane matrix. 339

Apart from direct sewage treatment, functionalized membranes could be used 340 341 more cost-effectively through combination with nanofiltration membrane-based separation to repair naphthenic acid in water containing highly concentrated total 342 dissolved solids (TDS). As seen in Fig. 8(d), a nanofiltration membrane can remove 343 naphthenic acid from large volumes of produced water via pathway B, resulting in 344 permeation comprised of discharge quality water (<10 mg/L) that leaves the operating 345 unit via pathway A-1. Finally, the retentate stream should be treated by Fe_xO_v 346 functionalized membrane/PDS system (AOP, pathway A-2) to meet the emission 347 standards for naphthenic acid and discharge via pathway C. 348

Pollutants in the feed solution are limited near the catalyst surface when the feed passes through the active layer of the membrane by way of voids between the catalysts. In the surface reaction, the concentration of short-lived ROS is significantly higher than that of the bulk. Thus, the pollutants are constantly and rapidly removed from the reaction zone, leading to a method of recovery of potable water that is more feasible, energy-intensive, and cost-effective. However, the amount of Fe leaching was very high (see **Table 2**). Therefore, further research, including long-term stability tests and technoeconomic analysis, is needed to verify the feasibility of the combination strategy in practical application.





Fig. 8. Typical composite membrane used in filtration mode reaction systems based on cross-flow filtration: (a) top-section SEM images of pristine PVDF membrane and CoFe-NMTs-800/PVDF membrane, cross-section SEM image of CoFe-NMTs-800/PVDF membrane, and metal leaching concentration after five runs in CoFe-NMTs-800/PMS system (reprinted with permission from [52],

363 copyright 2021 Elsevier); (b) schematic representation of integration of nanofiltration membranes and 364 Fe_xO_y functionalized membranes for treatment of naphthenic acid from produced water (reprinted with 365 permission from [55], copyright 2017 Elsevier); (c) schematic depiction of the Flowing Bed Device 366 (reprinted with permission from [54], copyright 2018 ACS); and (d) cross-flow filtration apparatus with 367 light irradiation (reprinted with permission from [53], copyright 2019 Elsevier).

The carbon-based catalytic membrane is likely to become a substitute for metal 368 369 catalysts, thus avoiding secondary pollution arising from metal leaching into the treated 370 water. As discussed above, only three studies have employed carbon-based catalytic membranes in which the catalytically active phase is placed on top of a certain support 371 372 (Polytetrafluoroethylene (PTFE) [47, 56] or nylon [51]). Vieira et al. [23] conducted a study of N-doped rGO (rGO-N) nanocatalysts, during which rGO-N-PTFE partially 373 disintegrated during continuous operation and/or drying. By contrast, rGO-N-PVDFs 374 exhibited structural and catalytic stability, demonstrating resistance toward fouling 375 phenomena. However, the performance of the treatment process declined dramatically 376 377 when surface water was used instead of ultrapure water in an early trial.

378 **3. Specific materials systems**

Metallic glasses (MGs) have grown in popularity in the field of wastewater remediation catalysis due to their great catalytic activity, high strength, elasticity, superior corrosion and wear resistance properties, and unique soft/hard magnetism [57, 58]. MG ribbons prepared by melt-spinning usually exhibit high efficiency, reusability, and sustainability [59]. Moreover, melt-spinning techniques have proved cost-effective when applied to industrial-scale water remediation [57].

385	Liang et al. [60] manufactured various iron-based MGs and applied them to
386	persulfate activation systems. Unlike powder catalysts, MG ribbons present a metallic,
387	flexible appearance (Fig. 9(a)) benefiting ease of operation, low cost, and control of
388	excess reaction [60]. Moreover, as-obtained MGs in persulfate-AOPs have outstanding
389	reusability, exceeding Fe78Si9B13 MG [61, 62], Fe73.5Si13.5B9Cu1Nb3 MG [63], and
390	$Fe_{83}Si_2B_{11}P_3C_1$ MG by factors of 30, 10, and 35 (see Fig. 9(b)) [64]. Such a durable
391	and efficient environmental catalyst has great potential in practical wastewater
392	remediation. The exact mechanism by which atoms participate and electrons are
393	transferred in MGs with amorphous structures is poorly understood, especially when
394	MGs are used as a catalyst. Jia et al. [61] stated that persulfate activation can be
395	attributed to ferrous (Fe^{2+}) in solution rather than in solid form in a
396	Fe78Si9B13/PDS/ultraviolet-visible light (UV-Vis) reaction system. Even so, in a more
397	recent study [62], Liang et al. utilized ZVI as an electron donor to activate PDS and
398	generate •OH and ferrous ions via a four-electron pathway involving water oxidation
399	in Fe ₇₈ Si ₉ B ₁₃ MG. Further reaction of Fe ²⁺ with persulfate then produced SO ₄ \cdot
400	Similarly, in a Fe78Si9B13/PMS/UV-Vis reaction system, direct surface corrosion of
401	Fe ₇₈ Si ₉ B ₁₃ ribbons by PMS generated SO ₄ ^{•-} . As the reaction progressed, ZVI on the
402	$Fe_{78}Si_9B_{13}$ MG surface was consumed by persulfate to produce ROS (used for pollutant
403	removal), after which UV-Vis irradiation accelerated the surface corrosive process.
404	Buried Fe was gradually covered by SiO ₂ , which in turn gradually changed from Si on
405	the ribbon surface during persulfate activation, thus preventing further iron leaching.
406	During mechanical stirring, SiO2 was easily shaken off, meaning that Fe78Si9B13

407 ribbons could react with peroxide when necessary, thereby realizing the high reusability 408 of $Fe_{78}Si_9B_{13}$ ribbons. However, when the service time was over 30 cycles, the 409 $Fe_{78}Si_9B_{13}$ ribbon became gradually exhausted due to the lack of a SiO₂ layer to prevent 410 further iron leaching, causing secondary pollution of the dye solution [61].

In recent years, three-dimensional (3D) printing, also known as additive 411 412 manufacturing, has emerged as a novel method for simplifying the single process of material manufacture. Liang et al. [60] successfully prepared Fe-based MGs with 3D 413 diamond dodecahedron microstructure using selective laser melting (SLM) according 414 415 to a predesigned 3D computer-aided design model (Fig. 9(c)). Their results showed that 416 efficiency remained almost unchanged after being used repeatedly 45 times, and that the surface after use was still as fresh as the original MG matrix composite. The ultra-417 418 stable reusability of the MG matrix composite in persulfate-AOPs means that it currently has the greatest reusability and catalytic potential among prospective catalysts. 419 420 Moreover, it is likely that even higher reusability will be achieved in future.

Follow-up studies have focused on optimizing the catalytic performance of MGs by accurately regulating their chemical composition and atomic structure. Even so, the link between structural heterogeneity and catalytic performance of MGs still needs to be confirmed, and the mechanism (or origin) behind their high catalytic performance has yet to be identified.



426

427 Fig. 9. Typical metallic glasses used in persulfate-AOPs: (a) schematic diagram of melt-spinning process 428 for manufacturing glassy ribbons and an optical photograph of typical product (reprinted with permission 429 from [57], copyright 2019 Elsevier); (b) comparison of the catalytic stability of different iron-based 430 materials (reprinted with permission from [64], copyright 2019 Wiley); and (c) synthetic procedure, SEM 431 images, and reusability of as-produced Fe-based MG matrix composite (Fe-based MGPDS-45: the Fe-based 432 MGPDS-45 after 45-times use in PDS activation process; Fe-based MGFenton-45: the Fe-based MGPDS-45 after 43345-times use in Fenton-like reaction process) (reprinted with permission from [60], copyright 2020 434 Elsevier).

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435
           Aerogels are a class of highly porous lightweight materials with an average pore
436
      size in the tens of nanometers, and are sublimated from the liquid components of
      traditional gels (usually by freeze-drying or critical point drying) [65, 66]. Cellulose
437
      aerogels have wide application prospects due to their high specific surface area, uniform
438
      pore size distribution, biodegradability, recyclability, and low cost [65, 67]. As
439
      indicated in Table 3, ZIF-9 and ZIF-12 were decorated on cellulose aerogels with
440
      macroscopic 3D structure and low weight (Fig. 10(a)), and the aerogels then used to
441
      activate PMS effectively [68]. Carbon aerogels are a new class of carbonaceous
442
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materials that feature an interconnected framework, possess large specific surface areas,
and have a hierarchical pore structure. Co-doped carbon aerogels (CoCA) activate PMS
at lower activation energy, effectively removing organic pollutants while maintaining a
low metal ion leaching rate [69] (Table 3). As evident in Fig. 10(b), CoCA floats
beneath the surface of the aqueous solution and can be completely removed without
any change in form.

Flow-type configurations are suitable for continuous treatment of wastewater, thus 449 expanding the applicability of aerogels. However, traditional isotropic graphene 450 451 aerogels and foams contain randomly dispersed graphene sheets, which would cause erosion and seriously reduce the flux. Compared with isotropic CoFe₂O₄(*a*)graphene 452 hybrid aerogels (CFO@GA-I), anisotropic CoFe₂O₄@graphene hybrid aerogels 453 454 (CFO@GA-A) have higher flux, lower metal ion leaching concentration, and much better, stable catalytic performance (Table 3 and Fig. 10(c)) [70]. Moreover, CFO@GA 455 aerogels can be stacked together to meet complex application conditions (Fig. 10(d)). 456

457 Hydrogels have rigid but soft elastic networks that permeate one another, giving them higher mechanical strength and strain capacity than aerogels [71]. Among 458 hydrogels, hydrophilic material offers an appropriate support conducive to mass 459 transfer in water treatment, and which reduces the dissolution of metal ions [72]. 460 Polyacrylic acid (PAA) is a kind of ionic hydrogel with polar carboxyl groups (-COOH) 461 that exhibit high adsorption efficiency toward metal ions and strong interaction with 462 water. After successfully synthesizing a 3D composite hydrogel based on 463 CoOOH/graphene oxide (CoOOH/GO) and PAA hydrogel precursor, Yi et al. [73] 464

constructed an automatic water treatment system under laboratory conditions (Fig. 465 10(e)). Duan et al. [74] discovered the formation of chemical bonds between Co₃O₄ and 466 467 graphene in a 3D hierarchical Co₃O₄/graphene hydrogel composite with high specific surface area, stable structure, and significantly heterogeneous surface synergistic effect 468 (Table 3). Later, the dual network hydrogel consisted of two interpenetrating networks 469 470 with enhanced structural properties [75-77]. Meanwhile, Zhuang et al. [78] prepared a double-network hydrogel templated FeS/graphene (DMG) based on a double-network 471 hydrogel containing Fe. This not only facilitated the formation of high-quality graphene 472 at a low cost but also achieved intensive interactions between Fe and graphene, as 473 shown in Fig. 10(f). 474

Overall, immobilizing as-prepared nanocatalysts into hydrogel can reduce the leaching concentration of metal ions based on specific chemical bond formation, thus avoiding the loss of nanocatalysts from the reactor [78-80].



478

479 Fig. 10. Typical aerogels and hydrogels used in persulfate-AOPs: (a) photographs of ZIF-based hybrid

480 aerogels (reprinted with permission from [68], copyright 2018 Elsevier); (b) elimination of phenol under 481 different conditions, and photographs of CoCA in water (inset) (reprinted with permission from [69], 482 copyright 2020 Elsevier); (c) schematic illustration of the preparation of an anisotropic CoFe₂O₄@GA-483 A and its application for the continuing treatment of wastewater with a flow-type setup (reprinted with 484 permission from [70], copyright 2020 Elsevier); (d) plots of removal efficiencies of organic pollutants 485 for CoFe₂O₄@GA-A and CoFe₂O₄@GA-I at different flow rates, and a photograph of real-time catalytic 486 experiments using CoFe2O4@GA-A and stacked CoFe2O4@GA-As (each red arrow indicates a piece of 487 CoFe₂O₄@GA-A) (reprinted with permission from [70], copyright 2019 ACS); (e) schematic illustration 488 of degradation equipment flowchart based on CoOOH/GO hydrogel composite (reprinted with 489 permission from [73], copyright 2019 ACS); and (f) preparation routine and photographs of samples 490 (reprinted with permission from [78], copyright 2020 RSC).

Apart from the abovementioned support materials, many other uncommon supports, such as polymer sponges [81], metal plates [82-85], and sand [86, 87], have been studied for the immobilization of persulfate catalysts, as listed in **Table 4**. These materials have two benefits: easy procurement in massive quantities and cost-efficiency for large-scale procedures.

Using a sponge catalyst composed of polyvinyl alcohol (PVA) as support, a 496 497 chemically bonded Co₃O₄ nanoflower sponge (SP-50) was prepared with good mechanical and elastic properties, adjustable geometry, multi-porosity, and multi-498 499 dimensionality. As shown in Fig. 11(a), the catalytic sponge floats on water and, more 500 importantly, can be easily recycled. Due to the use of bonding materials or organic 501 adhesives that limit contact between catalyst and target matrix, many published works concerning immobilized catalysts for persulfate activation have recently focused on 502 503 direct in situ growth catalysts situated on metal plates. For instance, Hoffmann et al. [83] employed cobalt-doped Black TiO₂ nanotubes (Co-Black TNT) as PMS activators 504

to degrade organic pollutants (**Fig. 11(b)**). Moreover, stainless steel was used for costeffective bifunctional supports and catalysts after appropriate pretreatment, owing to its mechanical firmness, corrosion resistance, conductivity, and ease of scale-up (**Fig. 11(c)**) [88]. In another study, waste from a sandwich cathode containing LiMn_2O_4 was directly used as a catalyst to activate PMS for removal of organic pollutants in water, which were then entirely (and easily) collected from the reaction system (**Fig. 11(d**)) [84].

As previously remarked, the continuous flow reactor system has two notable 512 characteristics: ease of operation and low energy consumption, thus marking a 513 514 milestone in the practical use of AOPs. Considering pollutant removal performance and operation process cost (see Table 4), CoFe₂O₄ was placed onto a quartz sand support 515 516 (CoFe₂O₄-QS) and packed into a column reactor to activate PMS [86]. Similarly, a systematic study evaluated the feasibility of using a sand column reactor, consisting of 517 BFMO (i.e., Mn_{1.5}FeO_{6.35}) and sand, to activate PMS in situ for the treatment of 518 trichloroethylene-contaminated water (Fig. 11(e)) [87]. The current findings indicate 519 that BFMO is a very stable and long-acting catalyst for persulfate-based *in situ* chemical 520 oxidation (ISCO), which may be employed for groundwater remediation. 521



522

523 Fig. 11. Specific materials based on uncommon supports prepared for persulfate activation: (a) digital 524images of as-obtained SP-50 sponge cut into different geometrical shapes; SEM images of (1) SP-50 525 sponge and (2) SP-50; digital photograph of SP-50/PMS reactive process (reprinted with permission 526 from [81], copyright 2019 Wiley); (b) digital photograph of Co-Black TNT/PMS reactive process and 527 the activation mechanisms (reprinted with permission from [83], copyright 2019 ACS); (c) SEM images 528 and activation mechanisms of the stainless-steel/PMS system for degrading organic contaminants 529 (reprinted with permission from [85], copyright 2020 Elsevier); (d) recycling process of spent lithium-530 ion battery (reprinted with permission from [84], copyright 2020 ACS); and (e) schematic illustration of 531PMS-based in situ chemical oxidation process and the sand columns (5 cm internal diameter \times 50 cm 532 length) working mode (reprinted with permission from [87], copyright 2020 ACS).

533 **4. Electrocatalytic auxiliary systems**

Electrocatalytic treatment is conducted by applying a potential to the anode and 534cathode in a reactor. In this process, influent is used as the electrolyte, with chemicals 535 added as necessary to improve conductivity. Direct degradation of targeted pollutants 536 537 occurs through charge transfer on the electrode surface. Anode and cathode processes can also indirectly promote the removal of pollutants through reaction with 538 electrochemically generated ROS. Construction of an electrochemically-activated 539 540 persulfate process can be achieved by means of a sacrificial anode system, electric filtration system, and photoelectrocatalytic system, as shown in Fig. 2. These reaction 541 542 systems improve degradation efficiency while reducing power consumption and cost. 543 They are particularly applicable to decentralized processes because of their efficiency and stability at small scale and ease of automatic control by current/voltage adjustment. 544 Electrochemical systems with addition of iron ions (Fe^{2+} or Fe^{3+}) for persulfate 545 activation were initially implemented to remove organic pollutants [89-91]. It was 546 found unexpectedly that Fe²⁺ can regenerate from the cathodic reduction reaction in 547 Fered-Fenton and other electro-Fenton processes [89], thereby overcoming the problem 548 of Fe^{2+} regeneration after transformation to Fe^{3+} . Thus, the reaction systems could 549 550 possess continuous persulfate catalytic capability; however, a large amount of iron sludge would inevitably be produced. 551

Later, electrochemical enhancement of persulfate-AOPs, with iron sheets used as sacrificial anodes, was used to promote destruction of organic contaminants (**Table 5**). In the oxidation process, once a current was applied between the anode and cathode, a

555	predetermined amount of persulfate was then added to the reactor. Ferrous ions
556	produced by sacrificial iron anodes mediated the persulfate decomposition. In Fig. 2,
557	the production rate of Fe^{2+} is controlled by the positive current of the iron anode,
558	according to the reaction expressed by Eq. (1). Consumed Fe^{2+} is regenerated on the
559	cathode, satisfying Eq. (2). In turn, OH^- forms and may restore the pH value and redox
560	potential, thus inhibiting heavy metals from leaching into the subsurface, as expressed
561	by Eq. (3). Therefore, the iron electrode can be readily introduced into a polluted region
562	to control persulfate activation in situ, thus minimizing the potential loss of persulfate
563	during injection and transportation [92].

564
$$\operatorname{Fe} - 2e^- \to \operatorname{Fe}^{2+}$$
 (1)

565
$$Fe^{3+} + 2e^- \to Fe^{2+}$$
 (2)

566
$$2H_2O + 2e^- \rightarrow H_2 + OH^-$$
 (3)

This sacrificial anode reaction system has several important advantages: low cost, 567 substantially reduced energy consumption, and remarkably increased pollutant 568 degradation. However, the approach has been criticized due to the increased operating 569 570 cost incurred from disposal of the iron sludge byproduct [93, 94]. Song et al. [95] detected the electrochemical activation of PDS at the Ti/Pt anode, whereas Farhat et al. 571 [96] studied the PDS activation performance of a boron-doped diamond electrode. 572 From the foregoing, it was found that discharge is the dominant factor in the 573 electrochemical activation processes of PDS, which induces the generation of the PDS 574 transition state. Hence, the electrode only plays a role in electron transfer and does not 575 directly participate in persulfate activation. 576

577	In capacitive deionization (CDI), application of a direct current voltage that is
578	lower than the water breakdown voltage (1.23 V) on the porous electrode can induce
579	ions or charged organic groups in an aqueous solution to gather quickly on the surface
580	of the polarized electrode and attract oppositely charged species to their surfaces; this
581	phenomenon is called the illegal Larch process [97]. Due to their great conductivity,
582	large specific surface area, and chemical stability, CNTs have been widely used as
583	electrode materials for CDI to remove organic pollutants from wastewater [93, 98]. As
584	reported, multi-walled carbon nanotube (MWCNT) cathodes were synthesized by a
585	casting method using PVA as binder and graphite sheet as support [93]. As shown in
586	Fig. 12(a), during each operation, a certain amount of stock liquid was continuously
587	pumped into the cell by a peristaltic pump until the discharged liquid returned to the
588	electrochemical cell. Interaction between persulfate and carbon surface functional
589	groups has been found to play a remarkable role in persulfate-AOPs. Electrochemical
590	reactions usually occur on the electrode surface, and the generated free radicals are
591	usually adsorbed on the electrode surface, although they are difficult to disperse
592	thoroughly in the bulk solution [95]. However, as shown in Fig. 12(b), activation and
593	electro-adsorption of PDS on the surface of a porous carbon electrode can promote
594	electron transfer between the generated active substance and target pollutant, which is
595	conducive to the degradation of pollutants. Correspondingly, the MWCNT electrode
596	reduces the working voltage and enhances PDS activation performance to degrade
597	organic pollutants simultaneously. The results showed that organic compounds on the
598	electrode surface and the generated reaction species helped promote the electron
transfer progress through the synergistic effect of electro-adsorption of pollutants and



600 electrochemical activation of PDS.



Likewise, Han et al. [103] investigated an enhanced electric activated carbon fiber 612

599

613	(ACF)/ferric iron/PDS (ACF-E/Fe ³⁺ /PDS) process in which ACF served as a cathode.
614	The results showed that the ACF cathode did not play a substantial role in activating
615	PDS, and a large number of iron ions were deposited on the cathode surface, indicating
616	good adsorption performance. Liu et al. [100] investigated the influence of operational
617	conditions, including pH, electrode potential temperature, peroxydisulfate
618	concentration, and water matrix. As listed in Table 5, ACF-E/PDS achieved a high
619	pollutant removal rate of 98.78% in 30 min with high PDS concentration [103], proving
620	that sufficient PDS can efficiently and quickly degrade pollutants. Therefore, in the
621	ACF-E/PDS system, the economic benefits and environmental effects of PDS
622	consumption or iron sludge disposal require further research. As depicted in Fig. 12(c),
623	SEM images of ACFvirgin (virgin ACF) and ACFEPDS100 (electro PDS (E-PDS) reacted
624	ACF after reutilization of 100 times) presented relatively neat surfaces, except that PDS
625	oxidation caused the surface of ACF_{PDS50} to become cracked and rough (the case
626	corresponding to PDS reacted ACF after 50-times reutilization). This finding may be
627	attributed to electrons on the cathode reducing damage by ROS or PDS to ACF while
628	maintaining continuous generation of SO4 without depleting the electron supply
629	residues of ACF. Furthermore (see Table 5), addition of PMS evidently improved the
630	current in the MnFe ₂ O ₄ /carbon fiber paper (CFP) electrode [104] as well as in the
631	PDA/CF cathode [105], indicating that the reaction between PMS and MnFe ₂ O ₄ /CFP
632	or PDA/CF was energetically favorable. Moreover, the applied bias and photogenerated
633	electrons of the photoanode facilitated the formation of different valence state ions in
634	MnFe ₂ O ₄ , which activated PMS for SO ₄ induction and catalytic stability of the

635 $MnFe_2O_4/CFP$ cathode [104].

This kind of cathodic catalyst protection phenomenon also exists in cathodic 636 637 material regeneration, such as the *in situ* regeneration of phenol-saturated ACF by an electro-PDS process [99]. The surface of ACF_{PDS} (virgin ACF immersed in the PDS 638 639 system for 180 min) was attacked and became covered with a mass of attachments 640 because ACF acted as a catalyst rather than an initiator. Compared with ACF_{PDS}, the morphological characteristics and pore texture ACF_{EPDS} (virgin ACF immersed in PDS 641 with 1 A current applied for 180 min) and ACF_{initial} coincided, such that the pore 642 643 remained almost unchanged.

By comparison with conventional electrochemical regeneration, the E-PDS 644 process can regenerate exhausted ACF and mineralized desorption pollutants 645 646 simultaneously by activating PDS with much lower energy consumption (1/6). However, a large number of oxides and oligomers produced by anodic oxidation can be 647 re-adsorbed to carbon, resulting in a regeneration efficiency of only about 60%. What 648 649 is worse is that, compared with ACF_{Re-E-PDS-1} (phenol-saturated ACF regenerated in the E-PDS process for one cycle), the structure of ACF_{Re-E-PDS-4} (phenol-saturated ACF 650 651 regenerated in E-PDS process for four cycles) deteriorated severely, as shown in the SEM image in Fig. 12(d). Therefore, after undergoing regeneration four times, the 652 653 regeneration efficiency decreased to less than 40%. As reported, the electro-PMS (E-PMS) treatment progress is more suitable for the regeneration of activated carbon [101]. 654 Phenol-saturated activated CF was regenerated in situ using an electro PMS reaction 655 system, as shown in Fig. 12(d). This reaction system mineralized the desorbed 656

contaminants (81.90%) while consuming only one-tenth of the energy. Even after ten 657 cycles, regeneration remained effective at around 60% of the initial value, and cathodic 658 659 polarization during E-PMS regeneration effectively protected the physical structure and chemical properties of ACF. Nevertheless, ACF had a minor impact on PMS self-660 decomposition, and its role in E-PMS was distinct from that of the E-PDS process. 661 662 Therefore, there is an urgent need to conduct more systematic, deeper studies on the experimental setup, and reaction mechanisms of combined 663 performance, electrochemical and persulfate activation, which is considered a sustainable, efficient, 664 665 low-toxicity technique for the remediation of contaminated water.

Several studies have activated persulfate on a plate cathodic surface, but achieved 666 poor performance (see e.g. Zhang et al. [102]). Electrostatic repulsion tends to drive 667 668 persulfate anions away from the cathode because both anions and cathode are negatively charged. Given the poor breakdown of persulfate and the low creation of 669 radicals, the contaminants then degrade slowly. Two possible approaches to 670 overcoming this problem are to shorten the diffusion distance and to increase collision 671 and contact between persulfate anions and the cathode. Zhang et al. used carbonized 672 wood with well-ordered channels as the cathode (Table 5), and performed a set of 673 comparative experiments for a flow-by cathode (FBC) and a flow-through cathode 674 (FTC) (Fig. 12(e)) to confirm that the microchannels of the FTC could boost the 675 creation of radicals, and organics degradation. Cycling tests revealed that this FTC was 676 quite stable. As a result, activating persulfate in FTC is an effective technique for 677 increasing radical yield and availability. 678

679 The electro-activated persulfate process mainly involves an electron transfer reaction. Increases in current density and residence time tend to improve the number of 680 681 electrons transferred and enhance the efficiency of the electrochemical activation. Several issues remain unresolved for all electrochemical-persulfate reaction systems. 682 683 Future research should consider energy consumption, electrode manufacturing costs, 684 power consumption, persulfate consumption, and loss in treatment capacity. Future research should also consider how to avoid secondary pollution by excess PMS and its 685 associated reaction products, and how to recycle principal byproducts such as SO_4^{2-} . 686 Furthermore, such studies should not only be conducted in the laboratory but also 687 expanded to pilot scale. 688

689 **5. Challenges and outlook**

690 The integration of various conventional research disciplines, such as materials science for the creation of purpose-driven catalysts and water treatment engineering for 691 the construction of practical reactors, has led to the effective application of 692 nanoparticle-based AOPs for water remediation. Correspondingly, rapid advances have 693 been achieved over the past few years in the emerging field of persulfate-based 694 immobilized-catalyst systems. This review article summarizes current developments 695 concerning nanocatalyst immobilization in persulfate-AOPs for target contaminant 696 697 removal. Various immobilization techniques onto supports, including membrane-based reaction systems (immersion mode, filtration mode), electrocatalytic auxiliary systems, 698 699 and other supports (metallic glasses, aerogels, and hydrogels, or specific materials), are

700 discussed.

Compared with common nanocatalyst reaction systems, the immobilized-catalyst 701 702 system can bypass the separation problem to reduce scour and prevent aggregation by anchoring nanoparticles onto porous or large-particle carriers. As a result, great effort 703 704 has been devoted to exploring suitable support substances for nanocatalysts and 705 designing reactors that cope with the changing environment for targeted pollutant removal. Meanwhile, a series of studies have been carried out to gain insight into the 706 persulfate activation mechanism. Even so, considerable challenges remain regarding 707 708 high-performance reactors and the practical applications of persulfate-based AOPs. 709 To ensure excellent activation performance and high reusability of next-generation 710 multifunctional treatment systems, it is necessary to develop advanced reactors,

711 incorporating advances in materials science and a fundamental understanding of key mechanisms. For example, direct evidence is still lacking for the outer- and inner-sphere 712 connection between nanocatalysts and supporting materials. Meanwhile, interactions 713 remain uncertain among catalysts, persulfate, and targeted pollutants. Although 714 715 laboratory studies have been undertaken to develop immobilized catalysts with simple recycling operation and excellent catalytic performance, the application and 716 717 commercialization of such technology is quite low in more complicated situations. Future studies are expected to employ persulfate-AOPs at pilot and semi-industrial 718 scales with the goal of reactor design and the focus on engineering issues. 719

In terms of the prospects for persulfate-based immobilized-catalyst systems, we
propose the following foci:

722 (1) Determine a universal design principle by which to optimize the structure and catalytic performance of heterogeneous catalysts. In practice, the optimization of 723 724 electronic characteristics and elemental composition of nanoparticles plays a remarkable role in catalytic processes. Through careful material design and theoretical 725 726 calculations, it is possible to prepare a catalyst with amazing performance. Furthermore, 727 reaction active sites and reaction pathways to the catalyst can be fully understood. Theoretical calculation and *in situ* characterization are two powerful techniques to 728 advance reaction mechanisms, both of which are instructive in determining design and 729 730 preparation rules for high-performance materials. Moreover, many state-of-the-art nanoparticles are notable for environmental applications, but have yet to make a 731 significant impact in the field of water treatment. Covalent organic frameworks (COFs), 732 733 for example, are an attractive new form of porous organic nanomaterials with desirable properties, including a completely organic metal-free backbone, low mass density, well-734 defined topology, structural variety, high heat resistance, and permanent porosity. An 735 736 effective, facile method for fabricating flexible, free-standing pure COF membranes has been described in a previous study, thus allowing development of new forms of 737 738 membrane-based persulfate-AOPs [106]. Furthermore, based on the mononuclear nature of the catalytic site, single-atom catalysts possess superior atomic utilization 739 efficiency, thus inheriting the advantages of homogeneous and heterogeneous catalysts. 740 (2) Optimize the combination of active materials and supporting substances. The 741 catalyst preparation stage pertains to reactor design and systems engineering. Here the 742 activity and stability of catalysts are only two of the key factors. The goal is to improve 743

744 the effective utilization of persulfate-AOPs. In most cases, immobilized-catalyst systems are inherently mass transfer-limited. Correspondingly, the approach is based 745 746 on nanocatalysts with outstanding, stable catalytic capability, which exploit the maximized surface area of the nanoscale active material and the support material 747 748 architecture. Additional studies should thus reveal the relationship between the 749 excellent catalytic performance of nanocatalysts and the structural properties of their supports in order to guide reactor design in systems engineering. Given their 750 widespread applications, the as-expected immobilized catalysts must be manufactured 751 752 at industrial scale (in tons), resulting in a stable, mature market. All the foregoing advances, including catalytic performance, stability, flexibility, and cost-efficiency, are 753 754 aimed at the development of new reactors.

755 (3) Solve problems of decreased performance in various complex water matrices and formation of reaction byproducts. Most of the studies examined in this review 756 detected the removal effect of target pollutants using synthetic water to evaluate the 757 catalytic capability of catalysts, hence, the lack of background organic content. 758 However, due to competitive adsorption onto catalyst surfaces and radical scavenging 759 in an aqueous solution, natural organic matter (NOM) is commonly recognized to 760 reduce persulfate-AOP performance. The remarkable spatiotemporal changes that take 761 place in water quality parameters (e.g. target pollutant concentration, turbidity, various 762 coexisting ions, and pH) are inherent challenges that have often been overlooked at 763 laboratory scale. Despite efforts to recreate realistic settings, the absence of defined 764 experimental methodology has made it difficult to obtain a quantitative evaluation of 765

the actual processing effect of persulfate-AOPs. In turn, this has limited effective technology transfer and commercialization. It should be noted that the majority of the research reviewed herein focused on the degradation of single or a few types of pollutants. In actual sewage, many types of pollutants co-exist, and so the cooperative inhibition of different types of pollutants merits further in-depth research. Hence, future studies are expected to employ persulfate-AOPs at pilot- and semi-industrial scales, aimed at improved reactor design while focusing on engineering aspects.

(4) *Reasonable evaluation of treatment effect of the reaction system*. Much work 773 has yet to be done in properly assessing the viability and industrialization of 774 immobilized catalysts in terms of cost and life-cycle impacts (which are mostly 775 unpredictable and unclear at this early stage of research). Although new studies on 776 777 persulfate-based AOPs for water treatment are often reported nowadays, these numerous studies and proposed technology combinations pose great challenges for the 778 assessment of AOPs. The challenges include operating costs (e.g., energy consumption, 779 780 and chemical inputs), general practicality (e.g., physical footprint, oxidation byproduct production, and impact on multiple microbial subsistence), and sustainability (e.g., 781 resource use, and carbon footprint). Future studies are likely to confirm the economic 782 benefits and environmental consequences of persulfate-based AOPs. For this purpose, 783 life-cycle analysis is required, which involves evaluating energy usage, natural 784 resources, and chemical products related to emissions to air, soil, and water, as well as 785786 considering potential trade-offs in actual environmental remediation.

787

788 **Declaration of Interest Statement**

The authors declare that they have no known competing financial interests or
personal relationships that could have appeared to influence the work reported in this
paper.

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1161 Figure captions

Fig. 1. Heterogeneous activation mechanism of persulfates, and challenges tonanocatalysts in persulfate-based-AOPs

Fig. 2. Construction strategy for persulfate activation systems based on immobilized
 nanocatalysts

Fig. 3. Typical composite membrane prepared via ceramic and polymeric substances, and 1166 then used in immersion mode reaction systems: (a) synthetic procedure for PAN-Co 1167 ceramic membrane, with SEM surface images of (a-1) initial Al₂O₃ membrane, and (a-2) 1168 1169 functionalized PAN-Co-C membrane, and SEM cross-section images of (a-3) initial 1170 Al₂O₃ membrane, and (a-4) functionalized PAN-Co-C membrane (reprinted with permission from [26], copyright 2019 Elsevier); (b) synthetic procedure for LDH@PVDF 1171 membrane (reprinted with permission from [27], copyright 2020 Elsevier); and (c) 1172 synthetic procedure for NSC-Fe@PVDF membranes, with (c-1) digital photograph of 1173 NSC-Fe@PVDF membrane and (c-2) color changes of Orange II in NSC-1174 Fe@PVDF/PMS system (reprinted with permission from [28], copyright 2017 Elsevier). 1175 Fig. 4. Typical composite membrane prepared from nanofibers through filtration, and 1176 1177 used in immersion mode reaction systems: (a) synthetic procedure, (b) SEM image of Co/Fe bi- MOFs/CNFs membrane (reprinted with permission from [32], copyright 2020 1178 Elsevier); and (c) schematic representation of magnetic nanocellulose membrane 1179 preparation and PMS activation process (reprinted with permission from [33], copyright 1180 1181 2020 Elsevier).

Fig. 5. Typical composite membrane prepared from electrospun nanofibers, and used in
immersion mode reaction systems: (a) synthetic procedure for metallic Cu-doped C/SiO₂

nanofibers (CINMs) by sol-gel electrospinning method; (b) SEM image of α-Fe@carbon 1184 ENFs (reprinted with permission from [38], Copyright 2017 RSC); (c) SEM image of 1185 1186 CINMs; and (d) optical photograph showing that the CINMs could be folded into a paper crane without any fracturing (reprinted with permission from [39], copyright 2019 RSC). 1187 1188 Fig. 6. Schematic illustration of reaction mechanism for organic removal by (a) Co/Fe bi-MOFs/cellulose NFs membrane/PMS system (reprinted with permission from [32], 1189 copyright 2020 Elsevier), and (b) NSC-Fe@PVDF/PMS system (reprinted with 1190 1191 permission from [28], copyright 2017 Elsevier).

Fig. 7. Typical composite membranes used in filtration mode reaction systems based on 1192 vacuum filtration: (a) synthetic procedure, SEM images, and water treatment method for 1193 1194 ZIF-67/PAN membrane (reprinted with permission from [50], copyright 2017 Elsevier); (b) synthetic procedure, SEM images, digital photos and water treatment method for 1195 CoCu LDH-CGF membrane and pristine CGF membrane. (reprinted with permission 1196 1197 from [27], copyright 2020 Elsevier); and (c) schematic diagram of the experimental setup under recirculation mode (configuration A) and continuous mode (configuration B). 1198 (reprinted with permission from [23, 47], copyright 2019 and 2020 Elsevier); the digital 1199 1200 photograph depicts elements in the filtration reaction system with recirculation and continuous modes (reprinted with permission from [51], copyright 2020 Elsevier). 1201

Fig. 8. Typical composite membrane used in filtration mode reaction systems based on cross-flow filtration: (a) top-section SEM images of pristine PVDF membrane and CoFe-NMTs-800/PVDF membrane, cross-section SEM image of CoFe-NMTs-800/PVDF membrane, and metal leaching concentration after five runs in CoFe-NMTs-800/PMS system (reprinted with permission from [52], copyright 2021 Elsevier); (b) schematic representation of integration of nanofiltration membranes and Fe_xO_y functionalized membranes for treatment of naphthenic acid from produced water (reprinted with
permission from [55], copyright 2017 Elsevier); (c) schematic depiction of the Flowing
Bed Device (reprinted with permission from [54], copyright 2018 ACS); and (d) crossflow filtration apparatus with light irradiation (reprinted with permission from [53],
copyright 2019 Elsevier).

Fig. 9. Typical metallic glasses used in persulfate-AOPs: (a) schematic diagram of melt-1213 spinning process for manufacturing glassy ribbons and an optical photograph of typical 1214 1215 product (reprinted with permission from [57], copyright 2019 Elsevier); (b) comparison of the catalytic stability of different iron-based materials (reprinted with permission from 1216 [64], copyright 2019 Wiley); and (c) synthetic procedure, SEM images, and reusability of 1217 as-produced Fe-based MG matrix composite (Fe-based MGPDS-45: the Fe-based MGPDS-45 1218 after 45-times use in PDS activation process; Fe-based MGFenton-45: the Fe-based MGPDS-1219 45 after 45-times use in Fenton-like reaction process) (reprinted with permission from [60], 1220 copyright 2020 Elsevier). 1221

Fig. 10. Typical aerogels and hydrogels used in persulfate-AOPs: (a) photographs of ZIF-1222 1223 based hybrid aerogels (reprinted with permission from [68], copyright 2018 Elsevier); (b) 1224 elimination of phenol under different conditions, and photographs of CoCA in water (inset) (reprinted with permission from [69], copyright 2020 Elsevier); (c) schematic illustration 1225 of the preparation of an anisotropic CoFe₂O₄@GA-A and its application for the 1226 continuing treatment of wastewater with a flow-type setup (reprinted with permission 1227 from [70], copyright 2020 Elsevier); (d) plots of removal efficiencies of organic pollutants 1228 1229 for CoFe₂O₄@GA-A and CoFe₂O₄@GA-I at different flow rates, and a photograph of real-time catalytic experiments using CoFe₂O₄@GA-A and stacked CoFe₂O₄@GA-As 1230 (each red arrow indicates a piece of CoFe₂O₄@GA-A) (reprinted with permission from 1231

[70], copyright 2019 ACS); (e) schematic illustration of degradation equipment flowchart
based on CoOOH/GO hydrogel composite (reprinted with permission from [73],
copyright 2019 ACS); and (f) preparation routine and photographs of samples (reprinted
with permission from [78], copyright 2020 RSC).

1236 Fig. 11. Specific materials based on uncommon supports prepared for persulfate activation: (a) digital images of as-obtained SP-50 sponge cut into different geometrical 1237 shapes; SEM images of (1) SP-50 sponge and (2) SP-50; digital photograph of SP-1238 50/PMS reactive process (reprinted with permission from [81], copyright 2019 Wiley); 1239 (b) digital photograph of Co-Black TNT/PMS reactive process and the activation 1240 mechanisms (reprinted with permission from [83], copyright 2019 ACS); (c) SEM images 1241 1242 and activation mechanisms of the stainless-steel/PMS system for degrading organic contaminants (reprinted with permission from [85], copyright 2020 Elsevier); (d) 1243 recycling process of spent lithium-ion battery (reprinted with permission from [84], 1244 copyright 2020 ACS); and (e) schematic illustration of PMS-based in situ chemical 1245 oxidation process and the sand columns (5 cm internal diameter \times 50 cm length) working 1246 mode (reprinted with permission from [87], copyright 2020 ACS). 1247

1248 Fig. 12. Electrocatalytic auxiliary systems constructed for persulfate activation: (a) schematic diagram of electrochemical activation of PDS and aniline degradation 1249 experiment (reprinted with permission from [93], Copyright 2018 Elsevier); (b) proposed 1250 mechanism of organic pollutant removal by asymmetric quasi capacitive deionization 1251 (AQCDI)/PDS/1.2V system (R represents the organic molecule and X represents the 1252 active sites in MWCNTs) (reprinted with permission from [98], copyright 2019 Elsevier); 1253 (c) SEM images of the ACF in different reaction systems (reprinted with permission from 1254 [99, 100], copyright 2018 and 2020 Elsevier); (d) schematic representation of ACF 1255

- 1256 Regeneration experimental setup (reprinted with permission from [101], copyright 2020
- 1257 ACS); and (e) schematic diagram of the E-PMS activation mechanism via FTC and FBC
- strategy (reprinted with permission from [102], copyright 2020 ACS).
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- 1260

Catalytic component and		Dellecteret were even	Metal leaching	Fabrication	Regeneration	Reaction
support material	Experimental conditions	Pollutant removal	(mg/L)	method	method	mode
Co embedded carbon (dip-	Membrane weight: 100 mg	Over 90%	[Co]=0.05	Dip-coating and	Not studied	Batch mode
coating)	Transmembrane pressure: 1 bar			carbonization		Immersion
Al ₂ O ₃ (20 nm pore size)	[Sulfamethoxazole]0=10 mg/L			method		
[26]	[PMS] ₀ =0.1 g/L					
	<i>T</i> =room temperature					
	pH _{solution} =not reported					
	<i>t</i> =60 min					
NSC-Fe	[Orange II] ₀ =20 mg/L	98% (in 1st cycle)	[Fe]=0.037	Phase inversion	Filtered and	Batch mode
PVDF	V=250 mL	~78% (in 4 th cycle)		technique	washed with	Magnetic
[28]	[PDS]0=0.6 g/L				ultrapure	stirring
	<i>T</i> =25 °C				water after	
	pH _{solution} (unadjusted)				each cycle	
	<i>t</i> =150 min					
	Single piece of membrane (24 cm ²)					
CoCu LDH	[Sulfamethoxazole]0=10 mg/L	Over 90% (from 1st	[Co]=0.044,	Phase inversion	Washed with	Batch mode
PVDF	V=100 mL	cycle to 10 th cycle)	[Cu]=0.026	technique	deionized	Magnetic
[27]	[PMS] ₀ =150 mg/L		(nanocatalysts		water and	stirring
	<i>T</i> =25 °C		[Co]=0.157,		ethanol after	
	pH _{solution} =5.77 (unadjusted)		[Cu]=0.174)		each cycle	
	<i>t</i> =60 min					
	Single piece of membrane $(5 \times 10 \text{ cm}^2)$ (catalyst					

Table 1. Summary of recent studies on catalytic membranes for persulfate activation in batch mode

	7.00 wt.%)					
CuO@CuS	[Organics] ₀ =10 mg/L	83.4% (Tetracycline),	[Cu]=1.664	Phase inversion	Washed with	Batch mode
PVDF	V=100 mL	about 50%	(nanocatalysts	technique	ethanol after	Magnetic
[107]	[PDS]0=0.4 g/L	(Enrofloxacin), about	[Cu]=2.147)		each cycle	stirring
	<i>T</i> =25 °C	45% (Ciprofloxacin),				
	pH _{solution} =7.34 (unadjusted)	40.8% (Lomefloxacin)				
	<i>t</i> =60 min					
	Single piece of membrane $(5 \times 5 \text{ cm}^2)$ (catalyst					
	20.00 wt.%)					
Co/Fe bi-MOFs	Single piece of membrane with 20 mg catalyst	100% (in 1st cycle)	Not reported	Vacuum filtration	Rinsed and	Batch mode
CNFs as fiber support and	V=100 mL	60% (in 5 th cycle)			freeze-dried	Immersion
unspecified organic substrate	[Tetrabromobisphenol A]0=50 mg/L					
(0.22 µm pore size) as	[PMS] ₀ =0.1 mM					
membrane support	<i>T</i> =room temperature					
[32]	$pH_{solution}=7.5$					
	<i>t</i> =30 min					
Fe ₃ O ₄	V=100 mL	Not reported	Not reported	In situ co-	Not studied	Batch mode
CNFs	[Rhodamine B] ₀ =20 mg/L			precipitation		Magnetic
[33]	[PMS] ₀ =1.0 g/L			method and		stirring
	T and pH _{solution} not reported			filtration		
	<i>t</i> =300 min					
a-Fe@carbon composite NFs	Membrane weight=10 mg	100% (in 1 st cycle)	Not reported	Electrospinning	Not illustrated	Batch mode
[38]	[Methyl blue] ₀ =10 mg/L	90% (in 5 th cycle)		method and		Magnetic
	V=100 mL			carbonization in an		stirring

	[PMS]0=0.5 g/L			N ₂ atmosphere		
	<i>T</i> =25 °C			environment		
	pH _{solution} (unadjusted)					
	<i>t</i> =15 min					
Metallic Cu-doped C/SiO ₂	Membrane weight=0.3 g/L	95% (in 1 st cycle)	[Cu]=0.18	Electrospinning	Washed with	Batch mode
nanofibers (CINMs)	[Tetracycline] ₀ =50 mg/L	Over 90% (in 5 th cycle)	(pH=7, after 10	method and	deionized	Magnetic
[39]	V=10 mL		min)	carbonization in an	water and	stirring
	[PDS] ₀ =0.3 g/L		[Cu]=0.37	N ₂ atmosphere	ethanol, dried	
	<i>T</i> =55 °C		((pH=7, after 40	environment	in an air-	
	pHsolution=9 (adjusted)		min)		circulating	
	<i>t</i> =40 min					
Co-Al ₂ O ₃ NFs membrane	Membrane weight=10 mg (catalyst 11.00 wt.%)	100%	$[Co]=0.10 \pm 0.4$	Electrospinning	Not studied	Batch mode
[41]	[Bisphenol A] ₀ =20 mg/L		$[A1]{=}0.09\pm0.09$	method		Mechanical
	<i>V</i> =10 mL					stirring
	[PMS] ₀ =1 mM					
	<i>T</i> =25 °C					
	pH _{solution} =7 (buffered)					
	<i>t</i> =40 min					
Pt-Al ₂ O ₃ NFs membrane	Membrane weight=1.0 g/L (catalyst 6 wt.%)	100% 97% and 88% (in	No Pt leaching	Electrospinning	Not illustrated	Batch mode
[42]	<i>V</i> =10 mL	the 1st, 2nd and 3rd cycle,	[Al]=0.37	method		Rotary shake
	[Bisphenol A] ₀ =20 mg/L	respectively)				
	[PMS] ₀ =2 mM	100% (stored for one				
	<i>T</i> =room temperature	week)				
	pH _{solution} =7.0 (buffered)	97% (stored for one				
	<i>t</i> =20 min	month)				

		87% (stored for one				
		year)				
	Membrane weight=1.0 g/L (catalyst 6 wt.%)	100%	Not reported	Electrospinning	Not illustrated	Batch mode
	<i>V</i> =10 mL			method		Mechanical
	[Bisphenol A] ₀ =20 mg/L					stirring
	[PMS] ₀ =2 mM					
	<i>T</i> =room temperature					
	pH _{solution} =7.0 (buffered)					
	<i>t</i> =20 min					
Ag-LCF	Membrane 30 cm long (catalyst 61.5 wt.%)	Over 90% (in the 1^{st} to	Not reported	Combined phase	Not illustrated	Batch mode
Initial spinning mixture	[Methyl blue] ₀ =10 ppm	4 th cycles)		inversion and		Surface flow
composed of Ag-LCF powder,	<i>Q</i> =26 mL/min	Less than 70% (in 5 th		sintering method		
polyethersulfone (PESF), and 1-	[PMS] ₀ =0.6 mM	cycle)				
methyl-2-pyrrolidinone (NMP)	T, t , and pH _{solution} not reported					
[43]						

Catalytic component and			Metal leaching	Fabrication	Regeneration	Filtration
support material	Experimental conditions	Pollutant removal	(mg/L)	method	method	mode
ZIF-67	Membrane weight=40 mg (catalyst 50 wt.%)	95.1% (in 1st cycle)	Not reported	In situ	Not illustrated	Batch mode
PAN (Mw=150,000)	[Acid yellow-17] ₀ =500 mg/L	93.9% (in 5 th cycle)		electrospinning		Magnetic
[46]	V=200 mL			method		stirring
	[PMS] ₀ =0.5 g/L					
	<i>T</i> =25 °C					
	pH _{solution} (unadjusted)					
	<i>t</i> =10 min					
CoCu LDH	About 60 s with -0.8 MPa	92.9% (about 60 s)	[Co]=1.605,	Vacuum filtration	Washed with	Batch
CGF as fiber support and PES as	V=100 mL	92.3% (about 60 s, in	[Cu]=1.919		deionized	filtrating
membrane support	[Sulfamethoxazole] ₀ =10 mg/L	10 th cycle)	(nanocatalysts		water and	mode
[27]	[PMS] ₀ =500 mg/L,		[Co]=0.157,		ethanol after	Pressure
	pH _{solution} =5.77 (unadjusted)		[Cu]=0.174)		each cycle	filtration
	<i>T</i> =25 °C					
	Single piece of membrane (12 cm ²)					
CoCu LDH	About 60 s with -0.8 MPa	95.81% (about 60 s)	[Co]=0.037,	Vacuum filtration	Washed with	Batch
PAN as fiber support and PES as	V=100 mL	94.66% (about 60 s, in	[Cu]=0.023		deionized	filtrating
membrane support	[Sulfamethoxazole] ₀ =10 mg/L	8 th cycle)	(nanocatalysts		water and	mode
[30]	[PMS] ₀ =0.65 mM	94.96% (about 60 s, in	[Co]=0.157,		ethanol after	Pressure
	pH _{solution} =5.77 (unadjusted)	10 th cycle)	[Cu]=0.174)		each cycle	filtration
	<i>T</i> =25 °C					
	Single piece of membrane (12 cm ²)					

 Table 2. Summary of recent studies on catalytic membranes for persulfate activation in a filtration system

spheres ν =50 mL 81% (6 th cycle)[Co]=0.15deionizedUnspecified organic substra[PDS]o=0.4 g/Lwater(0.22 µm pore size) as $\tau=25 \circ$ Cethanol sizemembrane supportpHsolution=77each cycle[108] $\tau=10$ minr=10 minMnsO4 embedded g-C3N4[4-Chlorophenol]o=12.9 mg/L90% (after 60 min)[Mn]=9.9Vacuum filtrationPTFE (0.22 µm pore size) as $\nu=20$ mL 80% (5 th cycle)deionizedmembrane support[PMS]o=0.15 g/L $water$ water[109] $\tau=25 \circ$ Cethanol sizeethanol sizepHsolution not reported $\mu=25 \circ$ Cethanol sizepHsolution not reported $\mu=25 \circ$ C $\mu=25 \circ$ CpHsolution not reported $\mu=25 \circ$ CpHsolution not reported $\mu=25 \circ$ CpHsolution not reported $\mu=25 \circ$ C<	filtratingandmodeafterPressurefiltrationwithBatchfiltratingandmodeafterPressure	
Unspecified organic substrate $(0.22 \ \mu m \text{ pore size})$ as membrane support $[PDS]_0=0.4 \ g/L$ water ethanol each cycle $(0.22 \ \mu m \text{ pore size})$ as $membrane support$ $T=25 \ ^{\circ}C$ ethanol each cycle $[108]$ $t=10 \ min$ $t=10 \ min$ MnsO4 embedded g-C3N4 $[4-Chlorophenol]_0=12.9 \ mg/L$ 90% (after 60 min) $[Mn]=9.9$ Vacuum filtrationMnsO4 embedded g-C3N4 $V=20 \ mL$ $80\% (5^{th} \ cycle)$ deionized waterPTFE (0.22 \ mm \ pore size) as membrane support $V=20 \ mL$ $80\% (5^{th} \ cycle)$ waterImmode the support $[PMS]_0=0.15 \ g/L$ $T=25 \ ^{\circ}C$ ethanol each cycle $[109]$ $T=25 \ ^{\circ}C$ ethanol each cycleethanol each cycle	and mode after Pressure filtration with Batch filtrating and mode after Pressure	
$(0.22 \ \mu\text{m} \text{ pore size})$ as $T=25 \ \circ\text{C}$ ethanolmembrane support $pH_{solution}=7$ each cycle $[108]$ $t=10 \ min$ $t=10 \ min$ MnsO4 embedded g-C3N4 $[4-Chlorophenol]_0=12.9 \ mg/L$ 90% (after 60 min) $[Mn]=9.9$ Vacuum filtrationWashedPTFE $(0.22 \ mm \text{ pore size})$ as $t=20 \ mL$ 80% (5 th cycle)deionizedmembrane support $[PMS]_0=0.15 \ g/L$ 80% (5 th cycle)water $[109]$ $T=25 \ \circ\ C$ ethanolethanol $pH_{solution}$ not reported $each cycleethanol$	after Pressure filtration with Batch filtrating and mode after Pressure	
membrane support pHsolution=7 each cycle [108] i=10 min i=10 min i=10 min MnsO4 embedded g-C3N4 [4-Chlorophenol]_0=12.9 mg/L 90% (after 60 min) [Mn]=9.9 Vacuum filtration Washed PTFE (0.22 mm pore size) as i=20 mL 80% (5 th cycle) deionized membrane support [PMS]_0=0.15 g/L water water [109] 1=25 °C ethanol ethanol pHsolution not reported pHsolution not reported etach cycle	e filtration with Batch filtrating and mode after Pressure	
[108] t=10 min Mn3O4 embedded g-C3N4 [4-Chlorophenol]_0=12.9 mg/L 90% (after 60 min) [Mn]=9.9 Vacuum filtration Washed PTFE (0.22 mm pore size) as t/=20 mL 80% (5 th cycle) deionized membrane support [PMS]_0=0.15 g/L water [109] T=25 °C ethanol pHsolution not reported pHsolution each cycle	with Batch filtrating and mode after Pressure	
Mn3O4 embedded g-C3N4[4-Chlorophenol]0=12.9 mg/L90% (after 60 min)[Mn]=9.9Vacuum filtrationWashedPTFE (0.22 mm pore size) as $\nu=20$ mL $80\% (5^{th} cycle)$ deionizedmembrane support[PMS]0=0.15 g/Lwater[109] $T=25$ °CethanolpHsolution not reportedpHsolution terportedeach cycle	with Batch filtrating and mode after Pressure	
PTFE (0.22 mm pore size) as V=20 mL 80% (5 th cycle) deionized membrane support [PMS]0=0.15 g/L water [109] T=25 °C ethanol pHsolution not reported pHsolution terported each cycle	and mode after Pressure	
membrane support[PMS]_0=0.15 g/Lwater[109]T=25 °CethanolpHsolution not reportedeach cycle	and mode after Pressure	
[109] T=25 °C ethanol = pH _{solution} not reported each cycle	after Pressure	
pH _{solution} not reported each cycle		
	e filtration	
<i>t</i> =60 min		
Ni-Co encapsulated N-doped $[Ibuprofen]_0=500 \ \mu g/L$ $\sim 70\%$ (after 20 min) $[Ni]=0.13$ Vacuum filtration Washed	with Semi-	
CNTs <i>V</i> =200 mL 100% (after 80 min) [Co]=0.18 deionized	continuou	15
PTFE (0.45 mm pore size) as [PMS] ₀ =0.1 g/L ~70% (after 80 min, in (after 80 min) water	after mode (un	nder
membrane support $T=25 ^{\circ}\text{C}$ 4^{th} cycle) each cycle	ycle; recirculat	ion)
[110] pH _{solution} =7.2 (buffered) after the t	third Under grav	vity
t=20 min (each recirculation) cycle, the	used	
catalyst	was	
heated	in	
argon	at	
350 °Cfor	r 3 h.	
N-doped rGO [Phenol] ₀ =5 mg/L or [Oxalic acid] ₀ =30 mg/L Phenol 30% (after 6.5 Metal free Vacuum filtration Without	Continuo	us
PTFE (0.45 mm pore size) as $Q=1.5 \text{ mL/min}$ h) regeneration	ion mode	

membrane support	[PDS]0=238 mg/L	Oxalic acid 65% (after			treatment	Pressure
[47]	<i>T</i> =25 °C	6.5 h)				filtration
	$pH_{solution} \mbox{=} \mbox{inherent} \ pH$ (~7.0 for phenol; 3.0 for					
	oxalic acid)					
	<i>t</i> =6.5 h					
rGO/CNTs	[Sulfamethoxazole] $_0=500 \ \mu g/L$	77% (after 3 h)	Metal free	Vacuum filtration	Without	Continuous
nylon substrate as membrane	<i>Q</i> =1.0 mL/min				regeneration	mode
support	[PDS] ₀ =1190 mg/L				treatment	Pressure
[51]	<i>T</i> =25 °C					filtration
	pH _{solution} not reported					
	<i>t</i> =3 h					
N-doped rGO	[Phenol] ₀ =47 mg/L	~80% (after 3 h)	Metal free	Vacuum filtration	Washed with	Continuous
PTFE (0.45 mm pore size) as	<i>Q</i> =1.5 mL/min				deionized	mode
membrane support	[PDS]0=238 m/L				water	Pressure
[56]	<i>T</i> =25 °C					filtration
	pH _{solution} =6.5					
	<i>t</i> =3 h					
rGO-ion nanoparticle	[Trichloroethylene] ₀ =0.2 mM	~85(over 17h)	Iron leaching was	Vacuum filtration	Without	Continuous
PVDF membrane support	Transmembrane pressure=0.4 bar		around 8%		regeneration	mode
[111]	[PDS] ₀ =2 mM				treatment	Pressure
	<i>T</i> =23 °C					filtration
	$pH_{solution}=7$					
	<i>t</i> =3 h					

Co-TPML	[Disphanal Al-0 2:1]	>000/	[Co]<0.1 µg/L	Vacuum filtration	Not illustrated	Continuous
PVDF membrane support	[Bisphenol A] ₀ =0.2µM	<i>></i> 90%	[00] 10.1 µg/L	vacuum mitation	1 tot mustrated	mode
	Transmembrane pressure=0.5 bar					Drossuro
[43]	[PMS] ₀ =10 mM					Clu d'
	<i>T</i> =20 °C					filtration
	pH _{solution} =3.5 (unadjusted)					
	<i>t</i> =1 h					
CoFe alloy and CoFe ₂ O ₄	V=100 mL	Tetracycline 99.2% (70	[Co]=0.015,	Phase invasion	Washed with	Batch
nanoparticles encapsulated in	[Tetracycline, Bisphenol A or Phenol] ₀ =30 mg/	min), Bisphenol A	[Fe]=0.004	technique	deionized	filtrating
N-doped microtube	L or [Orange G] ₀ =50 mg/L	98.7% (60 min), Phenol			water and	mode
composites (CoFe-NMTs)	[PMS] ₀ =0.3 g/L	99.5 (70 min) and			ethanol and	Pressure
PVDF as membrane substrate	pH _{solution} not reported	Orange G 100% (50			then dried in a	filtration
[52]	<i>T</i> =30 °C	min)			vacuum after	
	[catalyst] ₀ =0.1 g/L	Tetracycline over 95%			each cycle	
		(60 min, in 5 th cycle)				
ZIF-67	Membrane weight no reported (catalyst 31.8	TOC removal efficiency	Not reported	In situ self-	Without	Semi-
PP membrane support	wt.%)	of 82.2% (Methyl blue)		assembly approach	regeneration	continuous
[53]	Filtration pressure=0.1 MPa	and 83.5% (Methyl			treatment	mode (under
	Light gourge Veren large (200 W)	orange) (in 1st cycle)				recirculation)
	Light source. Action ramp (500 w)	73.3% (Methyl blue)				Pressure
	[Methyl blue or Methyl orange] ₀ =20 mg/L	and 82.0% (Methyl				filtration
	V=300 mL	orange) (in 1st cycle)				
	[PMS] ₀ =0.3 mM					
	T, t and pH _{solution} not reported					
a-Fe ₂ O ₃	Membrane, 3.8×1.6 cm ² , with catalyst of ~7.5	100% (Q=3 mL/h, after	Not reported	Vacuum filtration	Without	Continuous

bacterial cellulose	mg	84 h)			regeneration	flowing	bed
[54]	<i>Q</i> =3, 6, 9 mL/h	93% (<i>Q</i> =6 mL/h, after			treatment	state	
	[Rhodamine B] ₀ =10 mg/L each	62 h)					
	[PMS] ₀ =0.4 g/L	More than 87% (<i>Q</i> =9					
	Light source: Xenon lamp with a 400 nm cutoff	mL/h, after 42 h)					
	filter						
	T, t and pH _{solution} not reported						
Fe _x O _y	Time: 24 h (for 8 h in a cycle)	50% (in 1 st cycle)	Iron leaching was	In situ	Not illustrated	Batch mo	ode
PVDF as membrane substrate	<i>V</i> =50 mL	15% (in 2 nd cycle)	around 14.4%,	polymerization, ion		Surface fle	ow
[55]	[Naphthenic acids]0=48 mg/L		12.3%, and 16.2%	exchange,			
	[PDS] ₀ =17 mM		in three cycles,	reduction, and			
	pH _{solution} =5		respectively.	controlled oxidation			
	<i>T</i> =23 °C						
	Single piece of membrane (13.2 cm ² , Iron						
	loading: 12 g/m ²)						
	Average flux=2 LMH	44% (in 1st pass)	Not reported	In situ	Not illustrated	Continuo	us
	[Naphthenic acids]0=48 mg/L	42% (in 2 nd pass)		polymerization, ion		mode	
	[PDS] ₀ =5000 mg/L (added in every cycle)			exchange,		Pressure	
	pH _{solution} =5			reduction, and		filtration	
	<i>T</i> =23 °C			controlled oxidation			
	Single piece of membrane (13.2 cm ² , Iron						
	loading: 12 g/m ²)						
rGO-N	Membrane weight=23 mg (catalyst 6.4 wt.%)	54% (Ofloxacin), 77%	[Mn]=9.9	Knife cast technique	Without	Continuo	us
PVDF as membrane substrate	$Q=0.1 \text{ mL min}^{-1}$	(Ciprofloxacin) and			regeneration	mode	

[23]	[Ofloxacin, Ciprofloxacin and Enrofloxacin,	91% (Enrofloxacin)	treatment	Pressure
	simultaneously]0=100 µg/L each	(after 24 h)		filtration
	[PDS] ₀ =25 mg/L			
	<i>T</i> =room temperature			
	pH _{solution} =inherent pH (5.9)			
	<i>t</i> =24 h			

Catalytic component and	Experimental conditions	Catalytic Performance and	Regeneration	Motel leasting (mg/L)
support material	Experimental conditions	Stability	method	Mietai leaching (ing/L)
ZIF-9	[P-nitrophenol] ₀₌ 20 mg/L	About 90% (from 1 st to 3 rd cycle)	Washed with	[Co]=0.60 (the 1 st cycle)
Cellulose aerogels	[PMS] ₀₌₆₀₀ mg/L		deionized water	[Co]=0.50 (the 2 nd cycle)
[68]	[ZIF-9@GEL]0=600 mg/L			[Co]=0.30 (the 3 rd cycle)
	pH _{solution} =6 (adjusted)			
	<i>t</i> =130 min			
	<i>T</i> =25 °C			
ZIF-12	[P-nitrophenol] ₀₌ 20 mg/L	About 85% (from 1^{st} to 3^{rd} cycle)	Washed with	[Co]=0.75 (the 1 st cycle)
Cellulose aerogels	[PMS] ₀₌ 600 mg/L		deionized water	[Co]=0.60 (the 2 nd cycle)
[68]	[ZIF-12@GEL]0=600 mg/L			[Co]=0.45 (the 3 rd cycle)
	pH _{solution} =6 (adjusted)			
	<i>t</i> =130 min			
	<i>T</i> =25 °C			
Cobalt and Co ₃ O ₄	[Phenol] ₀₌ 20 mg/L	87% (in 1 st cycle)	Without regeneration	[Co]=0.014 (the 1 st cycle)
Carbon aerogels	[PMS] ₀₌ 2.6 mM	84% (in 2 nd cycle)	treatment	[Co]=0.011 (the 2 nd cycle)
[69]	[Composite] ₀ =1.0 g/L	67% (in 3 rd cycle)		[Co]=0.004 (the 3 rd cycle)
	$pH_{solution}$ =7.5 (adjusted and buffered)			
	<i>t</i> =60 min			
	<i>T</i> =25 °C			

Table 3. Recent studies on hydrogels and aerogels in persulfate-AOPs system

CoFe ₂ O ₄			[Indigo carmine] ₀ =50 ppm	100% (30 h, 60 mL/h)	Without regeneration	Not reported
Anisotropic	graphene	Hybrid	[PMS] ₀ =0.2 g/L	91% (25 h, 90 mL/h)	treatment	
Aerogels			[CFO@GA-A] ₀ =165.1 mm ² ×11.4 mm	85% (21 h, 120 mL/h)		
[70]			pH _{solution} unadjusted			
			T not reported			
CoFe ₂ O ₄			[Indigo carmine] ₀ =50 ppm	100% (4 h, 60 mL/h) and 41%	Without regeneration	Not reported
Isotropic	graphene	Hybrid	[PMS] ₀ =0.2 g/L	(subsequent 10 h, 60 mL/h)	treatment	
Aerogels			[CFO@GA-I] ₀ =165.1 mm ² ×11.4 mm	Drop to 35% (within 5 h, 120 mL/h)		
[70]			pH _{solution} unadjusted			
			T not reported			
BiOI			[Methylparaben] ₀ =50 mg/L	99% (90 min, with light irradiation)	Without regeneration	Not reported
p(HEA-APTM) hydrogel			[PMS] ₀ =30 mM	More than 80% (180 min, in dark)	treatment	
[71]			[Composite] ₀ =2.0 g/L			
			Xenon lamp (500 W)			
			pH _{solution} and T not reported			
CoOOH/GO	[Rhodamine B] ₀ =20 mg/L	About 85% (in 1 st cycle)	Calcination treatment	In Fig. 10(e)		
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PAA hydrogel	<i>V</i> =1 L	Above 60% (in 10 th cycle)				
[73]	[PMS] ₀ =0.15 mM					
	$200\ mg\ Co(NO_3)_2{\cdot}6H_2O$ was used for CoOOH					
	preparation					
	pH _{solution} =6.0 (unadjusted)					
	Flow rate=200 mL/min					
	t=5 min					
	T not reported					
C03O4	[Orange II] ₀ =0.2 mM	100% (from 1^{st} to 5^{th} cycle)	Dried in a vacuum	[Co]=0.360		
Graphene hydrogel	[PMS] ₀ =1 mM		oven overnight			
[74]	[Composite] ₀ =0.05 g/L		without any treatment			
	Neutral pH _{solution} (buffered)					
	<i>t</i> =90 min					
	<i>T</i> not reported					
Carbon black nano-spheres	[Acetaminophen] ₀ =0.1 mM	76.8% (in 1 st cycle)	Not illustrated	No metal		
(CBNS)/Fe ₃ O ₄	[PMS] ₀ =1.0 mM	66.8% (in 5 th cycle)				
Calcium alginate hydrogel matrix	[Composite] ₀ =0.3 g/L					
[80]	pH _{solution} =5.5 (unadjusted)					
	<i>t</i> =60 min					
	T not reported					

FeS	[Tetracycline] ₀ =100 mg/L	92.2% (in 1 st cycle)	Shaken in distilled Not reported
Graphene hydrogel	[PMS] ₀ =2 mM	88.3% (in 5 th cycle)	water for 6 h
[78]	[Composite] ₀ =1.0 M		
	pH _{solution} =6 (unadjusted)		
	<i>t</i> =120 min		
	<i>T</i> =25 °C		

Catalytic component and support material	Experimental conditions	Catalytic Performance and Stability	Regeneration method	Metal leaching (mg L ⁻¹)
C03O4	[Acid Orange 7] ₀ =0.3 mM	100% (15 min, in 4 th cycle)	Washed with distilled	[Co]=0.0118-0.066 (over eight runs)
Polymer sponge	[PMS] ₀ =3 mM	100% (21 min, in 6 th cycle)	water and ethanol and	
[81]	[Composite] ₀ =0.6 g/L	100% (24 min, in 8 th cycle)	dried in a vacuum after	
	pH _{solution} =7 (adjusted and buffered)		each cycle	
	<i>T</i> =25 °C			
TiO ₂	[Ciprofloxacin]0=10 mg/L	99.16% (from 1^{st} to 5^{th} cycle)	Dried	Not reported
Ti plate	[PMS] ₀ =0.5 mM	92% (in 6 th cycle)		
[82]	Xenon lamp (300 W)			
	pH _{solution} =6.3 (No description)			
	<i>t</i> =90 min			
	T not reported			
Co-Black TNT	[4-chlorophenol] ₀ =100 µM	100% (from 1^{st} to 15^{th} cycle)	Without regeneration	[Co]=0
Ti plate	[PMS] ₀ =1 mM		treatment	
[83]	pH _{solution} =7.0 (buffered)			
	<i>t</i> =30 min			
	T not reported			
Recycled active LiMn ₂ O ₄	[Ortho-phenylphenol]0=20 mg/L	100% (in 1 st cycle)	Washed with deionized	Not reported
Al foil in spent lithium-ion	[PMS]0=0.3 g/L	94.8% (in 10 th cycle)	water	
batteries	pH _{solution} not reported			
[84]	<i>t</i> =60 min			
	<i>T</i> =25 °C			

	Table 4.	Recent	studies on	persulfate-A	AOPs with	unusual	materials	as activators
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Surface-etched and N ₂ -annealed	[Orange II] ₀ =10 mg/L	100% (from 1^{st} to 3^{rd} cycle)	Washed with ethanol after	Not reported
stainless-steel mesh	[PMS]0=0.25 g/L		each cycle.	
Stainless-steel mesh	pH _{solution} unadjusted			
[85]	<i>t</i> =40 min			
	<i>T</i> =25 °C			
CoFe ₂ O ₄	V=1 L	Fresh composite:	Calcined in the muffle	Contrary to the batch reactor, the
Quartz sand	[Sulphachloropyridazine sodium]0=20 mg/L	Over 80% (from 0 to 360 min)	furnace at 300 °C for 4 h.	continuous flow reactor exhibited about
[86]	[PMS] ₀ =75 mg/L	Over 75% (from 360 to 480 min)		a quarter lower cobalt leaching.
	[Composite]0=0 g (1.0% CoFe2O4 loading)	Regenerated composite:		
	pH _{solution} =6.8 (adjusted)	Over 80% (from 0 to 120 min)		
	Flow rate=6 mL/min			
	T not reported			
Mn _{1.5} FeO _{6.35}	[Trichloroethylene] ₀ =20 mg/L	BFMO remained stable in the sand	Not reported	Not reported
Sand	[PDS] ₀ =8 mM	column throughout 115-day		
[87]	Column reactor (porosity of 25.7%) packed with	continuous flow test period.		
	sand (99.5 wt.%) and the BFMO catalysts (0.5 $$			
	wt.%)			
	$pH_{solution}=7.0$			
	Flow rate=1.47 L/d			
	T not reported			

Anodo	Cathada	Dof	Experimental conditions	Catalytic performance
Alloue	Cathode	Kel.	Experimental conditions	and stability
Fe sheet	Fe sheet	[112]	[Pentachlorophenol] ₀ =0.10 mM	75% (Mineralization
(4.2 cm×3 cm×0.5	(4.2 cm×3 cm×0.5		[PMS] ₀ =9.9×10 ⁻⁵ M	efficiency)
cm, 25.2 cm ²)	cm, 25.2 cm ²)		[NaCl]=1.7 mM	
			<i>t</i> =10 min	
			pH _{solution} =4.5 (unadjusted)	
			Current density=90 mA	
			T not reported	
			[Pentachlorophenol]0=0.10 mM	About 60% (mineralization
			[PDS] ₀ =9.9×10 ⁻⁵ M	efficiency)
			[NaCl]=1.7 mM	
			<i>t</i> =20 min	
			pH _{solution} =6.5 (unadjusted)	
			Current density=90 mA	
			T not reported	
Fe sheet	Graphite bar	[113]	[2,4,5-Trichlorophenoxyacetic	About 100%
(10 cm^2)			acid]0=0.10 mM	
			[PMS] ₀ =0.25 mM	
			[Na ₂ SO ₄]=50 mM	
			<i>t</i> =30 min	
			pH _{solution} not reported (unadjusted)	
			Current=10 mA	
			$T=23 \pm 2 \ ^{\circ}\mathrm{C}$	
Fe sheet	Mixed metal oxide	[92]	[Trichloroethylene]0=0.4 mM	More than 99%
(Cast gray iron, 76	sheet		[PDS] ₀ =5 mM	
mm×9.5 mm×3.2	(85 mm×15 mm×1.8		<i>t</i> =20 min	
mm)	mm, IrO ₂ /Ta ₂ O ₅		$pH_{solution}=5.6$ (unadjusted)	
	coating on titanium		Current=+100 mA	
	mesh type)		T not reported	
Graphite sheet	MWCNTs coating	[93]	[Aniline] ₀ =0.45 mM	98% (in the 1 st cycle)
(4.5 cm×4.5 cm)	graphite sheet		[PDS] ₀ =5.55 mM	89% (in the 9 th cycle)
	cathode		<i>t</i> =150 min	
	(with active		pH _{solution} not reported	

Table 5. Recent studies on electro-assistance persulfate-AOPs

	materials of ~ 85		Working voltage=-0.6 V	
	mg, 4.5 cm×4.5 cm)		T not reported	
Graphite sheet	MWCNTs coating	[98]	[Acyclovir]0=0.45 mM	Above 95% (from 1^{st} to 3^{rd}
(4.5 cm×4.5 cm)	graphite sheet		[PDS] ₀ =11.1 mM	cycle, negative polarization)
	cathode		<i>t</i> =120 min (positive polarization)	Above 95% (from 1^{st} to 11^{th}
	(with active		<i>t</i> =180 min (negative polarization)	cycle, negative polarization)
	materials of ~ 10		pH _{solution} not reported	
	mg, 4.5 cm×□4.5		Working voltage=1.2 V	
	cm)		T not reported	
Ti/Pt	ACF coating	[103]	[Carbamazepine] ₀ =0.04 mM	97.76% (in 1 st cycle)
(50 mm×35 mm×1	Titanium plate		[PDS] ₀ =2 mM	above 97% (in 10 th cycle)
mm)	cathode		[Fe ³⁺]=0.4 mM	
	(50 mm×35 mm×1		[Na ₂ SO ₄]=50 mM	
	mm)		<i>t</i> =30 min	
			pH _{solution} =3 (adjusted)	
			Current density=7.14 mA/cm ²	
			<i>T</i> =25 °C	
Pt-plating titanium	ACF coating Pt-	[100]	[Carbamazepine] ₀ =0.042 mM	98.78% (in 1 st cycle)
(50 mm×35 mm)	plating titanium		[PDS] ₀ =100 mM	97.35% (in 100 th cycle)
	cathode		<i>t</i> =30 min	
	(50 mm×35 mm)		pH _{solution} =3 (adjusted)	
			Working voltage=6 V	
			<i>T</i> =25 °C	
BiVO ₄ photoanode	MnFe ₂ O ₄ coating	[104]	[Bisphenol A] ₀ =10 mg/L	100% (in 1 st cycle)
$(1 \times 1 \text{ cm}^2)$	Carbon paper		[PMS] ₀ =1 mM	About 85% (in 5 th cycle)
	(CFP) cathode		<i>t</i> =90 min	
			pH _{solution} not reported	
			Working voltage=1 V	
			<i>T</i> =20 °C	
			Xenon lamp (300 W)	
BiVO4 photoanode	PDA coating	[105]	[Ofloxacin] ₀ =0.04 mM	100% (in 1 st cycle)
(16 cm^2)	carbon felt (CF)		[PMS] ₀ =2 mM	above 90% (in 5 th cycle)
	cathode		<i>t</i> =120 min	
	(16 cm^2)		$pH_{solution}=5$ (buffered)	
			Working voltage=1.5 V	
			T not reported	

		Xenon lamp (300 W)	
Platinum-plated	ACF coating Pt- [99]	[Phenol] ₀ =1600 mg/L	66% (in 1 st cycle)
titanium	plating titanium	[PDS]0=100 mM	34.12% (in 4 th cycle)
(5.0×3.5 cm)	cathode	[Na ₂ SO ₄]=0.2 M	
	(0.2 g, 5.0 cm×3.5	<i>t</i> =6 h	
	cm×3 mm)	pH _{solution} not reported (unadjusted)	
		Current intensity=1 A	
		<i>T</i> =25 °C	
Not reported	Carbonized wood [102]	[Phenol] ₀ =20 mg/L	97.9% (in 1 st cycle)
	cathode	[PMS] ₀ =6.51 mM	98.4% (in 2 nd cycle)
	(4.0 cm×2.0 cm×0.8	[Na ₂ SO ₄]=50 mM	98.0% (in 3 rd cycle)
	cm)	<i>t</i> =10 min	97.6% (in 4 th cycle)
		pH _{solution} =2.87 (unadjusted)	97.9% (in 5 th cycle)
		Current density=2.75 mA/cm ²	
		<i>T</i> =25 °C	